Regulations Compliance Report



Approved Document L1A, 2013 Edition, England assessed by Stroma FSAP 2012 program, Version: 1.0.4.23 Printed on 17 December 2019 at 15:54:53

Proiect Information:

Assessed By: Matthew Stainrod (STRO023501) Building Type: Semi-detached House

Dwelling Details:

NEW DWELLING DESIGN STAGETotal Floor Area: 81.12m²

Site Reference: Land off Impington Lane Plot Reference: 10-17-65487 Plot 25 (Type B)

Address: Plot 25 (Type B), Land off Impington Lane

Client Details:

Name: Hill Partnerships Ltd

Address: The Power House, Powdermill Lane, Waltham Abbey, EN9 1BN

This report covers items included within the SAP calculations.

It is not a complete report of regulations compliance.

1a TER and DER

Fuel for main heating system: Mains gas

Fuel factor: 1.00 (mains gas)

Target Carbon Dioxide Emission Rate (TER) 18.26 kg/m²

Dwelling Carbon Dioxide Emission Rate (DER) 13.98 kg/m² OK

1b TFEE and DFEE

Target Fabric Energy Efficiency (TFEE) 50.6 kWh/m²

Dwelling Fabric Energy Efficiency (DFEE) 46.7 kWh/m²

OK

2 Fabric U-values

| Element | Average | Highest | |
|---------------|------------------|------------------|----|
| External wall | 0.20 (max. 0.30) | 0.20 (max. 0.70) | OK |
| Party wall | 0.00 (max. 0.20) | - | OK |
| Floor | 0.12 (max. 0.25) | 0.12 (max. 0.70) | OK |
| Roof | 0.10 (max. 0.20) | 0.10 (max. 0.35) | OK |
| Openings | 1.33 (max. 2.00) | 1.40 (max. 3.30) | OK |

2a Thermal bridging

Thermal bridging calculated from linear thermal transmittances for each junction

3 Air permeability

Air permeability at 50 pascals 5.00 (design value)

Maximum 10.0 OK

4 Heating efficiency

Main Heating system: Database: (rev 453, product index 017958):

Boiler systems with radiators or underfloor heating - mains gas

Brand name: Vaillant Model: ecoFIT sustain 825

Model qualifier: VUW 256/6-3 (H-GB)

(Combi)

Efficiency 89.3 % SEDBUK2009

Minimum 88.0 % OK

Secondary heating system: None

Regulations Compliance Report



| 5 Cylinder insulation | | | |
|-------------------------------|------------------------|--------------------|----|
| Hot water Storage: | No cylinder | | |
| 6 Controls | | | |
| | | | |
| Space heating controls | TTZC by plumbing and e | lectrical services | OK |
| Hot water controls: | No cylinder thermostat | | |
| | No cylinder | | |
| Boiler interlock: | Yes | | OK |
| 7 Low energy lights | | | |
| Percentage of fixed lights wi | th low-energy fittings | 100.0% | |
| Minimum | | 75.0% | OK |
| 8 Mechanical ventilation | | | |
| Continuous extract system (| decentralised) | | |
| Specific fan power: | , | 0.19 0.18 | |
| Maximum | | 0.7 | OK |
| 9 Summertime temperature | | | |
| Overheating risk (East Angli | a): | Slight | OK |
| Based on: | , | • | |
| Overshading: | | Average or unknown | |
| Windows facing: North East | | 3.79m² | |
| Windows facing: South Wes | t | 7.1m² | |
| Ventilation rate: | | 4.00 | |
| | | | |
| 10 Key features | | | |
| Doors U-value | | 1 W/m²K | |
| Roofs U-value | | 0.1 W/m²K | |
| Party Walls U-value | | 0 W/m²K | |
| Floors U-value | | 0.12 W/m²K | |
| Photovoltaic array | | | |

Predicted Energy Assessment



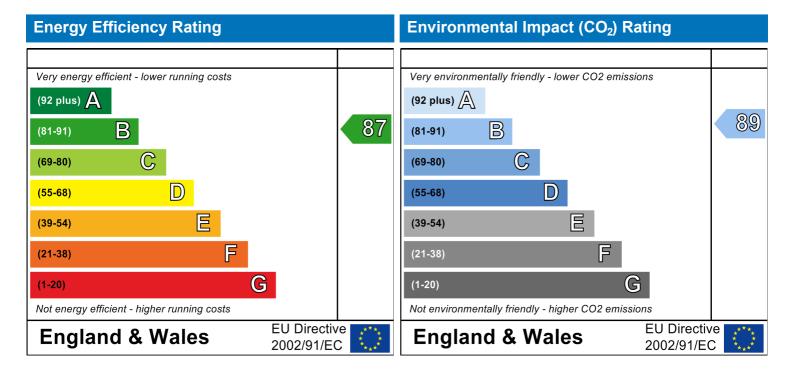
Plot 25 (Type B) Land off Impington Lane

Dwelling type:
Date of assessment:
Produced by:
Total floor area:

Semi-detached House 17 December 2019 Matthew Stainrod 81.12 m²

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2012 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO2) emissions.



The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be.

The environmental impact rating is a measure of a home's impact on the environment in terms of carbon dioxide (CO2) emissions. The higher the rating the less impact it has on the environment.

SAP Input



Property Details: 10-17-65487 Plot 25 (Type B)

Address: Plot 25 (Type B), Land off Impington Lane

Located in: England Region: East Anglia

UPRN:

Date of assessment: 17 December 2019
Date of certificate: 17 December 2019
Assessment type: New dwelling design stage

Transaction type: New dwelling
Tenure type: Unknown
Related party disclosure: No related party
Thermal Mass Parameter: Calculated 153.58
Water use <= 125 litres/person/day: True

PCDF Version: 453

Property description:

Dwelling type: House

Detachment: Semi-detached

Year Completed: 2019

Floor Location: Floor area:

Floor 0 40.56 m^2 2.4 m Floor 1 40.56 m^2 2.7 m

Living area: 19.7 m² (fraction 0.243)

Front of dwelling faces: North East

Opening types:

| Name: | Source: | Type: | Glazing: | Argon: | Frame: |
|------------|--------------|---------|--------------------------------|--------|--------|
| Front Door | Manufacturer | Solid | | | Wood |
| Front | Manufacturer | Windows | low-E, $En = 0.05$, soft coat | Yes | PVC-U |
| Rear | Manufacturer | Windows | low-E, $En = 0.05$, soft coat | Yes | PVC-U |

Storey height:

| Name: | Gap: | Frame Fa | actor: g-value: | U-value: | Area: | No. of Openings: |
|------------|--------------|----------|-----------------|----------|-------|------------------|
| Front Door | mm | 0.7 | Ō | 1 | 2.2 | 1 |
| Front | 16mm or more | 0.7 | 0.63 | 1.4 | 3.79 | 1 |
| Rear | 16mm or more | 0.7 | 0.63 | 1.4 | 7.1 | 1 |

Width: Type-Name: Location: Orient: Height: Name: External Wall North East Front Door 0 Front External Wall North East 0 0 External Wall South West 0 Rear 0

Overshading: Average or unknown

Opaque Elements:

| Type: | Gross area: | Openings: | Net area: | U-value: | Ru value: | Curtain wall: | Kappa: |
|---------------------|-------------|-----------|-----------|----------|-----------|---------------|--------|
| External Element | <u>ts</u> | | | | | | |
| External Wall | 92.82 | 13.09 | 79.73 | 0.2 | 0 | False | 60 |
| Roof - flat ceiling | 40.56 | 0 | 40.56 | 0.1 | 0 | | 9 |
| Ground Floor | 40.56 | | | 0.12 | | | 75 |
| Internal Element | <u>:S</u> | | | | | | |
| Stud Walls | 153.6 | | | | | | 9 |
| Ceiling | 40.56 | | | | | | 9 |
| Floor | 40.56 | | | | | | 18 |
| Party Elements | | | | | | | |
| Wall | 39.78 | | | | | | 45 |

SAP Input



| Iharmai | l bridges: |
|------------|-------------|
| IIICIIIIai | i biliuyes. |

| THEITIM DITUIES. USCI UCITICU (HIGINIGUALI SI VAIUCS) I VAIUC — VIVOZO | Thermal bridges: | User-defined (individual PSI-values) Y-Value = 0.0828 |
|--|------------------|---|
|--|------------------|---|

| | Length | Psi-value | | |
|------------|--------|-----------|-----|---|
| [Approved] | 8.66 | 0.3 | E2 | Other lintels (including other steel lintels) |
| [Approved] | 6.06 | 0.04 | E3 | Sill |
| [Approved] | 23.2 | 0.05 | E4 | Jamb |
| [Approved] | 18.2 | 0.16 | E5 | Ground floor (normal) |
| [Approved] | 18.2 | 0.07 | E6 | Intermediate floor within a dwelling |
| [Approved] | 10.4 | 0.06 | E10 | Eaves (insulation at ceiling level) |
| [Approved] | 7.8 | 0.24 | E12 | Gable (insulation at ceiling level) |
| [Approved] | 10.2 | 0.09 | E16 | Corner (normal) |
| [Approved] | 10.2 | 0.06 | E18 | Party wall between dwellings |
| | 7.8 | 0.16 | P1 | Ground floor |
| | 7.8 | 0 | P2 | Intermediate floor within a dwelling |
| | 7.8 | 0.12 | P4 | Roof (insulation at ceiling level) |

Ventilation:

Pressure test: Yes (As designed)

Ventilation: Decentralised whole house extract

Number of fans in Wetroom: Kitchen 1 Other 2

Ductwork:,

Approved Installation Scheme: False

Number of chimneys: 0
Number of open flues: 0
Number of fans: 0
Number of passive stacks: 0
Number of sides sheltered: 2
Pressure test: 5

Main heating system:

Main heating system: Boiler systems with radiators or underfloor heating

Gas boilers and oil boilers

Fuel: mains gas

Info Source: Boiler Database

Database: (rev 453, product index 017958) Efficiency: Winter 87.3 % Summer: 90.2

Brand name: Vaillant Model: ecoFIT sustain 825

Model qualifier: VUW 256/6-3 (H-GB)

(Combi boiler)

Underfloor heating, pipes in screed above insulation

Central heating pump: 2013 or later Design flow temperature: Unknown

Boiler interlock: Yes Delayed start

Main heating Control:

Main heating Control: Time and temperature zone control by suitable arrangement of plumbing and electrical

services

Control code: 2110

Secondary heating system:

Secondary heating system: None

Water heating:

Water heating: From main heating system

Water code: 901
Fuel :mains gas
No hot water cylinder

SAP Input



Solar panel: False

Others:

Electricity tariff: Standard Tariff
In Smoke Control Area: Unknown
Conservatory: No conservatory

Low energy lights: 100%

Terrain type: Low rise urban / suburban

EPC language: English Wind turbine: No

Photovoltaics: Photovoltaic 1

Installed Peak power: 0.75 Tilt of collector: 45°

Overshading: None or very little Collector Orientation: South West

Assess Zero Carbon Home: No



User Details: Matthew Stainrod STRO023501 **Assessor Name:** Stroma Number: Stroma FSAP 2012 **Software Version:** Version: 1.0.4.23 **Software Name:** Property Address: 10-17-65487 Plot 25 (Type B) Plot 25 (Type B), Land off Impington Lane Address: 1. Overall dwelling dimensions: Av. Height(m) Volume(m³) Area(m²) Ground floor 40.56 (1a) x 2.4 (2a) =97.34 (3a) First floor (1b) x 40.56 27 (2b) 109.51 (3b) Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+....(1n)81.12 Dwelling volume (3a)+(3b)+(3c)+(3d)+(3e)+....(3n)(5) 206.86 2. Ventilation rate: main secondary other total m³ per hour heating heating x 40 =Number of chimneys (6a) 0 0 0 0 0 x 20 = Number of open flues 0 0 0 0 0 (6b) Number of intermittent fans x 10 =(7a) 0 0 Number of passive vents x 10 =(7b) 0 0 Number of flueless gas fires x 40 =(7c)n Air changes per hour Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = \div (5) = 0 (8)If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16) Number of storeys in the dwelling (ns) (9) 0 Additional infiltration [(9)-1]x0.1 =(10)0 Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction 0 (11)if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35 If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0 (12)0 If no draught lobby, enter 0.05, else enter 0 0 (13)Percentage of windows and doors draught stripped (14)0 $0.25 - [0.2 \times (14) \div 100] =$ Window infiltration 0 (15)(8) + (10) + (11) + (12) + (13) + (15) =Infiltration rate 0 (16)Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area (17)5 If based on air permeability value, then $(18) = [(17) \div 20] + (8)$, otherwise (18) = (16)0.25 (18)Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used Number of sides sheltered (19)Shelter factor $(20) = 1 - [0.075 \times (19)] =$ 0.85 (20)Infiltration rate incorporating shelter factor $(21) = (18) \times (20) =$ (21)0.21

| (22)m= | 5.1 | 5 | 4.9 | 4.4 | 4.3 | 3.8 | 3.8 | 3.7 | 4 | 4.3 | 4.5 | 4.7 |
|--------|-----|---|-----|-----|-----|-----|-----|-----|---|-----|-----|-----|
| | | | | | | | | | | | | |

Jun

Jul

Aug

Sep

Oct

Nov

Dec

Infiltration rate modified for monthly wind speed

Mar

Apr

May

Feb

Monthly average wind speed from Table 7

Jan



| Wind Factor (22a)m = (22)m ÷ 4 | | | | | | | | | | | |
|---|--|--|---|---|---|---|----------|-------------------------------------|----------|--|---|
| (22a)m= 1.27 1.25 1.23 1. | 1 1.08 | 0.95 | 0.95 | 0.92 | 1 | 1.08 | 1.12 | 1.18 | | | |
| Adjusted infiltration rate (allowing for | or shelter and | d wind s | speed) = | (21a) x | (22a)m | - | | | - | | |
| 0.27 0.27 0.26 0.2 | | 0.2 | 0.2 | 0.2 | 0.21 | 0.23 | 0.24 | 0.25 | | | |
| Calculate effective air change rate in the state of the s | or the applic | cable ca | se | - | - | - | - | - | | | (23a) |
| If exhaust air heat pump using Appendix | N. (23b) = (23a) |) × Fmv (e | eguation (N | N5)) . othe | rwise (23b |) = (23a) | | | 0. | | (23b) |
| If balanced with heat recovery: efficiency | . , , , , | , | • | | , | , (, | | | 0. | | (23c) |
| a) If balanced mechanical ventila | _ | | | | | 2b)m + (| 23b) × [| 1 – (23c) | | , | (200) |
| (24a)m= 0 0 0 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 |] | | (24a) |
| b) If balanced mechanical ventila | tion without | heat red | covery (N | лV) (24b |)m = (22 | 2b)m + (| 23b) | | 1 | | |
| (24b)m= 0 0 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | (24b) |
| c) If whole house extract ventilati | on or positive | e input v | ventilatio | n from c | outside | • | • | | • | | |
| if (22b)m < 0.5 × (23b), then | (24c) = (23b) |); other | vise (24 | c) = (22b | o) m + 0. | .5 × (23b |) | 1 | 7 | | |
| (24c)m= 0.52 0.52 0.51 0. | | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | | | (24c) |
| d) If natural ventilation or whole h if (22b)m = 1, then (24d)m = | • | • | | | | 0.51 | | | | | |
| $\frac{11(220)111 - 1}{(24d)m} = 0 0 0$ | ` | 0 | 0 | 0.5 1 [(2 | 0 | 0.5] | 0 | 0 |] | | (24d) |
| Effective air change rate - enter (| l 24a) or (24b | or (24) | c) or (24 | d) in box | (25) | | | <u> </u> | J | | . , |
| (25)m= 0.52 0.52 0.51 0. | - | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |] | | (25) |
| | | | l | l | | | | 1 | 1 | | |
| 2 Heat leases and heat less name | 2001011 | | | | | | | | | | |
| 3. Heat losses and heat loss paral | | Net Ar | ea. | l I-valı | IA. | ΔΧΙΙ | | k-valu | a | ΔΧΙ | |
| | meter: enings m² | Net Ar A ,r | | U-valı W/m2 | | A X U (W/ | | k-value | | A X k | |
| ELEMENT Gross Ope | enings | | | | | | | | | kJ/K | |
| ELEMENT Gross Operation of the Gross area (m²) | enings | A ,r | m² x | W/m2 | K = | (W/ | | | | kJ/K | |
| ELEMENT Gross operation of the desired of the des | enings | A ,r | m² x x x 1/2 | W/m2 | = 0.04] = | (W/ 2.2 | | | | kJ/K | (26) |
| ELEMENT Gross operation of the second of the | enings | A ,r 2.2 3.79 | m ² x x1/2 x1/2 | W/m2 1 /[1/(1.4)+ | = 0.04] = | (W/ 2.2 5.02 | K) | | | kJ/K | (26) (27) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor | enings | A ,r 2.2 3.79 7.1 | m ² | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ | 0.04] = 0.04] = | (W/ 2.2 5.02 9.41 | K) | kJ/m²· | | kJ/K 3042 | (26) (27) (27) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor | enings m² | A ,r 2.2 3.79 7.1 40.56 | x10 | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ | 0.04] = 0.04] = = = = = = = = = = = = = = = = = = = | (W/ 2.2 5.02 9.41 4.8672 | K) | kJ/m²· | | kJ/K 3042 4783.8 | (26) (27) (27) (28) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 | enings m² | A ,r 2.2 3.79 7.1 40.56 | m ² | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ | 0.04] = 0.04] = = = = = = = = = = = = = = = = = = = | (W/ 2.2 5.02 9.41 4.8672 15.95 | K) | kJ/m ² · 75 | | 3042 4783.8 365.04 | (26) (27) (27) (28) (29) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 Roof 40.56 | enings m² | A ,r 2.2 3.79 7.1 40.56 79.73 | m ² | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ | 0.04] = 0.04] = = = = = = = = = = = = = = = = = = = | (W/ 2.2 5.02 9.41 4.8672 15.95 | K) | kJ/m ² · 75 | | 3042 4783.8 365.04 | (26) (27) (27) (28) (29) (30) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 Roof 40.56 Total area of elements, m² | enings m² | A ,r 2.2 3.79 7.1 40.56 79.73 40.56 173.9 | m ² | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ 0.12 0.2 0.1 | 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] | (W/ 2.2 5.02 9.41 4.8672 15.95 4.06 | K) | kJ/m ² · 75 60 | | 3042 4783.8 365.04 | (26) (27) (27) (28) (29) (30) (31) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 Roof 40.56 Total area of elements, m² Party wall | enings m² | A ,r 2.2 3.79 7.1 40.56 79.73 40.56 173.9 39.78 | m ² | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ 0.12 0.2 0.1 | 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] | (W/ 2.2 5.02 9.41 4.8672 15.95 4.06 | K) | kJ/m ² · 75 60 9 | | 3042 4783.8 365.04 1790.1 | (26) (27) (27) (28) (29) (30) (31) (32) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 Roof 40.56 Total area of elements, m² Party wall Internal wall ** | enings m² | A ,r 2.2 3.79 7.1 40.56 79.73 40.56 173.9 39.78 | x1/2 x1/2 x1/4 x1/4 x1/4 x1/4 x1/4 x1/4 x1/4 x1/4 | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ 0.12 0.2 0.1 | 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] = 0.04] | (W/ 2.2 5.02 9.41 4.8672 15.95 4.06 | K) | 75 60 9 45 | | 3042 4783.8 365.04 1790.1 1382.4 730.08 | (26) (27) (27) (28) (29) (30) (31) (32) (32c) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 Roof 40.56 Total area of elements, m² Party wall Internal wall ** Internal floor | enings m² 13.09 0 | A ,r 2.2 3.79 7.1 40.56 79.73 40.56 173.9 39.78 40.56 40.56 | m ² | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ 0.12 0.2 0.1 | 0.04] = 0.04] = 0.04] = = = | (W/ 2.2 5.02 9.41 4.8672 15.95 4.06 | K) | 75 60 9 45 9 | k | 3042 4783.8 365.04 1790.1 1382.4 730.08 | (26) (27) (27) (28) (29) (30) (31) (32) (32c) (32d) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 Roof 40.56 Total area of elements, m² Party wall Internal wall ** Internal floor Internal ceiling * for windows and roof windows, use effective area (m²) | enings m² 13.09 0 | A ,r 2.2 3.79 7.1 40.56 79.73 40.56 173.9 39.78 40.56 40.56 | x1/2 x1/3 x1/4 x1/3 x x1/4 x1/4 x1/4 x1/4 x1/4 x1/4 x1/4 x1 | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ 0.12 0.2 0.1 | | (W/ 2.2 5.02 9.41 4.8672 15.95 4.06 | K) | 75 60 9 45 9 | k | 3042 4783.8 365.04 1790.1 1382.4 730.08 365.04 | (26) (27) (27) (28) (29) (30) (31) (32) (32c) (32d) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 Roof 40.56 Total area of elements, m² Party wall Internal wall ** Internal floor Internal ceiling * for windows and roof windows, use effective ** include the areas on both sides of internal | enings m² 13.09 0 | A ,r 2.2 3.79 7.1 40.56 79.73 40.56 173.9 39.78 40.56 40.56 | x1/2 x1/3 x1/4 x1/3 x x1/4 x1/4 x1/4 x1/4 x1/4 x1/4 x1/4 x1 | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ 0.12 0.2 0.1 | K | (W/ 2.2 5.02 9.41 4.8672 15.95 4.06 | K) | 75 60 9 45 9 18 9 | K | 3042 4783.8 365.04 1790.1 1382.4 730.08 365.04 | (26) (27) (28) (29) (30) (31) (32) (32c) (32d) (32e) |
| ELEMENT Gross area (m²) Doors Windows Type 1 Windows Type 2 Floor Walls 92.82 Roof 40.56 Total area of elements, m² Party wall Internal wall ** Internal floor Internal ceiling * for windows and roof windows, use effective ** include the areas on both sides of internal Fabric heat loss, W/K = S (A x U) | enings m² 13.09 0 | A ,r 2.2 3.79 7.1 40.56 79.73 40.56 173.9 39.78 40.56 40.56 ilue calculations | x1/2 x1/2 x1/2 x1/2 x1/2 x1/2 x1/2 x1/2 | W/m2 1 /[1/(1.4)+ /[1/(1.4)+ 0.12 0.2 0.1 | K | (W/ 2.2 5.02 9.41 4.8672 15.95 4.06 | K) | 75 60 9 45 9 18 9 | K | 3042 4783.8 365.04 1790.1 1382.4 730.08 365.04 | (26) (27) (27) (28) (29) (30) (31) (32) (32c) (32d) (32e) (33) |

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can be used instead of a detailed calculation.



| Therm | al bridge | es : S (L | x Y) cal | culated | using Ap | pendix l | < | | | | | | 14.4 | (36) |
|-----------------|-----------------|----------------|-------------|-------------|-------------|-------------------------|-------------|------------------------|------------|------------------------|-----------------------------|---------|---------|----------|
| | | | are not kn | own (36) = | = 0.05 x (3 | 1) | | | | | | | | _ |
| | abric hea | | | | | | | | . , | (36) = | | | 55.9 | (37) |
| Ventila | | | | l monthly | ĺ | _ | | 1 . | | | 25)m x (5) | | 1 | |
| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | (00) |
| (38)m= | 35.56 | 35.2 | 34.84 | 34.13 | 34.13 | 34.13 | 34.13 | 34.13 | 34.13 | 34.13 | 34.13 | 34.13 | | (38) |
| Heat tr | | oefficier | nt, W/K | | , | | | | (39)m | = (37) + (| 38)m | | ı | |
| (39)m= | 91.46 | 91.1 | 90.74 | 90.03 | 90.03 | 90.03 | 90.03 | 90.03 | 90.03 | 90.03 | 90.03 | 90.03 | | _ |
| Heat Id | oss para | meter (H | ILP). W | /m²K | | | | | | Average = = (39)m ÷ | Sum(39) _{1.} · (4) | 12 /12= | 90.3 | (39) |
| (40)m= | 1.13 | 1.12 | 1.12 | 1.11 | 1.11 | 1.11 | 1.11 | 1.11 | 1.11 | 1.11 | 1.11 | 1.11 | | |
| | ! | | | <u> </u> | <u> </u> | | ļ | | / | Average = | Sum(40) ₁ . | 12 /12= | 1.11 | (40) |
| Numbe | er of day | s in mor | nth (Tab | le 1a) | | | | | | | | | | |
| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |
| (41)m= | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | (41) |
| | | | | | | | | | | | | | | |
| 4. Wa | iter heat | ing ener | gy requi | irement: | | | | | | | | kWh/ye | ear: | |
| Δeeum | ed occu | pancy, N | d | | | | | | | | | 40 | 1 | (42) |
| | | | | [1 - exp | (-0.0003 | 49 x (TF | A -13.9 |)2)] + 0.0 | 013 x (T | ΓFA -13. | | 48 | | (42) |
| | A £ 13.9 | • | | | | | | | | | | | | |
| | | | | | | | | (25 x N) to achieve | | se target o | | .19 | | (43) |
| | | | | | ater use, h | | | .0 40111010 | a water de | o target e | • | | | |
| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |
| Hot wate | er usage ir | | day for ea | <u> </u> | Vd,m = fac | ctor from 7 | Table 1c x | | • | | ļ | | | |
| (44)m= | 102.51 | 98.78 | 95.05 | 91.33 | 87.6 | 83.87 | 83.87 | 87.6 | 91.33 | 95.05 | 98.78 | 102.51 | | |
| | | | | | | | | ! | | | m(44) ₁₁₂ = | | 1118.27 | (44) |
| 0, | | | | | | | | Tm / 3600 | | | ables 1b, 1 | c, 1d) | | |
| (45)m= | 152.02 | 132.96 | 137.2 | 119.61 | 114.77 | 99.04 | 91.77 | 105.31 | 106.57 | 124.2 | 135.57 | 147.22 | | _ |
| If instan | taneous w | ater heatir | na at noint | of use (no | hot water | storage) | enter () in | boxes (46) | | Γotal = Su | m(45) ₁₁₂ = | • | 1466.23 | (45) |
| | - | | | | | | | | | 40.00 | 00.04 | 00.00 | 1 | (46) |
| (46)m= Water | 22.8 storage | 19.94 loss: | 20.58 | 17.94 | 17.22 | 14.86 | 13.77 | 15.8 | 15.99 | 18.63 | 20.34 | 22.08 | | (46) |
| | • | | includir | ng any so | olar or W | WHRS | storage | within sa | ame vess | sel | | 0 | | (47) |
| If com | munity h | eating a | nd no ta | ınk in dw | /elling, e | nter 110 | litres in | (47) | | | | | l | |
| Otherv | vise if no | stored | hot wate | er (this in | ncludes i | nstantar | neous co | mbi boil | ers) ente | er '0' in (| 47) | | | |
| | storage | | | | | | | | | | | | | |
| | | | | | or is kno | wn (kWh | n/day): | | | | | 0 | | (48) |
| Tempe | erature fa | actor fro | m Table | 2b | | | | | | | | 0 | | (49) |
| | | | _ | , kWh/ye | | | | (48) x (49) | = | | | 0 | | (50) |
| • | | | | - | loss facto | | | | | | | ^ | 1 | (51) |
| | | eating s | | | le 2 (kWl | ı/ııtı C /Uð | 'y <i>)</i> | | | | | 0 | | (51) |
| | - | from Tal | | | | | | | | | | 0 | | (52) |
| Tempe | erature fa | actor fro | m Table | 2b | | | | | | | | 0 | | (53) |
| | | | | | | | | | | | | | • | |



| Energy lost from water storage, kV Enter (50) or (54) in (55) | Vh/year | | | (47) x (51) |) x (52) x (| 53) = | | 0 | | (54) (55) |
|--|--|--|--|--|--|--|--|---|---------------|--|
| Water storage loss calculated for e | each month | | | ((56)m = (| 55) × (41)r | n | | U | | (33) |
| (56)m= 0 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (56) |
| If cylinder contains dedicated solar storage | , (57)m = (56)m x | ([(50) – (H | H11)] ÷ (50 | 0), else (5 | 7)m = (56) | m where (| H11) is fro | m Append | ix H | |
| (57)m= 0 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (57) |
| Primary circuit loss (annual) from | Γable 3 | | | | | | | 0 | | (58) |
| Primary circuit loss calculated for e | • | , , | , | , , | | | | | | |
| (modified by factor from Table H | | i | | | | | | | 1 | (EO) |
| (59)m= 0 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (59) |
| Combi loss calculated for each mo | ```````` | | | | | | | | ı | |
| (61)m= 23.66 21.3 23.41 22 | 2.46 23.07 | 22.16 | 22.8 | 22.97 | 22.32 | 23.27 | 22.75 | 23.61 | | (61) |
| Total heat required for water heating | | for each | month | (62)m = | 0.85 × (| 45)m + | (46)m + | (57)m + | (59)m + (61)m | |
| (,, | 2.07 137.84 | 121.2 | 114.57 | 128.28 | 128.89 | 147.47 | 158.32 | 170.83 | | (62) |
| Solar DHW input calculated using Appendix | | | | | | contributi | on to wate | er heating) | | |
| (add additional lines if FGHRS and | | | | | r i | 0 | | | [| (62) |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | (63) |
| Output from water heater | 0.07 407.04 | 404.0 | 444.57 | 400.00 | 400.00 | 447.47 | 450.00 | 470.00 | ı | |
| (64)m= 175.68 154.26 160.61 14 | 2.07 137.84 | 121.2 | 114.57 | 128.28 | 128.89 | 147.47 | 158.32 | 170.83 | 4740.04 | (64) |
| | ", " 0.05 | / FO OF | (45) | | out from wa | | | | 1740.01 |](04) |
| Heat daine from Water heating KW | | | | | | | | | | |
| Heat gains from water heating, kW | | - - | | | - | _ , | | · · · |] | (GE) |
| (65)m= 56.46 49.53 51.47 45 | 5.39 43.93 | 38.47 | 36.21 | 40.76 | 41.02 | 47.11 | 50.76 | 54.85 | | (65) |
| (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (6 | 5.39 43.93 65)m only if cy | 38.47 | 36.21 | 40.76 | 41.02 | 47.11 | 50.76 | 54.85 | | (65) |
| (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m. 5. Internal gains (see Table 5 and | 5.39 43.93 65)m only if cy | 38.47 | 36.21 | 40.76 | 41.02 | 47.11 | 50.76 | 54.85 | | (65) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in c | 6.39 43.93 65)m only if cy | 38.47 38.47 Inder is | 36.21 s in the c | 40.76 dwelling | 41.02 or hot w | 47.11 ater is fr | 50.76 om com | 54.85 munity h | | (65) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m. 5. Internal gains (see Table 5 and Metabolic gains (Table 5), Watts Jan Feb Mar A | 43.93 43.93 65)m only if cy d 5a): Apr May | 38.47 sinder is | 36.21 s in the c | 40.76 dwelling | 41.02 or hot w | 47.11 ater is fr | 50.76 om com | 54.85 munity h | | |
| (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (6 5. Internal gains (see Table 5 and Metabolic gains (Table 5), Watts Jan Feb Mar A (66)m= 149.03 149.03 149.03 14 | 43.93 43.93 65)m only if cy d 5a): Apr May 9.03 149.03 | 38.47 dinder is Jun 149.03 | 36.21 s in the c | 40.76 dwelling Aug 149.03 | 41.02 or hot w Sep 149.03 | 47.11 ater is fr | 50.76 om com | 54.85 munity h | | (65) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m. 5. Internal gains (see Table 5 and Metabolic gains (Table 5), Watts Jan Feb Mar A (66)m= 149.03 149.03 149.03 14 Lighting gains (calculated in Appen | 43.93 43.93 65)m only if cy d 5a): Apr May 9.03 149.03 andix L, equation | 38.47 Viinder is Jun 149.03 Dn L9 or | 36.21 S in the country Jul 149.03 L9a), a | 40.76 dwelling Aug 149.03 lso see | 41.02 or hot was Sep 149.03 Table 5 | 47.11 ater is fr Oct 149.03 | 50.76 om com Nov 149.03 | 54.85 munity h | | (66) |
| (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (6 5. Internal gains (see Table 5 and Metabolic gains (Table 5), Watts Jan Feb Mar A (66)m= 149.03 149.03 149.03 14 Lighting gains (calculated in Appendication) 53.52 47.53 38.66 29 | 43.93 43.93 65)m only if cydd 5a): Apr May 9.03 149.03 andix L, equation 0.26 21.88 | 38.47 dinder is Jun 149.03 on L9 or 18.47 | 36.21 S in the C Jul 149.03 L9a), a 19.96 | Aug 149.03 Iso see | 41.02 or hot w Sep 149.03 Table 5 34.82 | 47.11 ater is fr Oct 149.03 | 50.76 om com | 54.85 munity h | | |
| (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (6 5. Internal gains (see Table 5 and Metabolic gains (Table 5), Watts Jan Feb Mar A (66)m= 149.03 149.03 149.03 14 Lighting gains (calculated in Apper (67)m= 53.52 47.53 38.66 29 Appliances gains (calculated in Apper (calcu | 43.93 Apr May 9.03 149.03 Apr May 9.03 149.03 Apr May 9.03 149.03 Apr May 9.03 Apr | 38.47 Ilinder is Jun 149.03 on L9 or 18.47 ation L1 | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Tal | 47.11 ater is fr Oct 149.03 44.21 ble 5 | 50.76 om com Nov 149.03 | 54.85 munity h Dec 149.03 | | (66) (67) |
| (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (6 5. Internal gains (see Table 5 and Metabolic gains (Table 5), Watts Jan Feb Mar A (66)m= 149.03 149.03 149.03 14 Lighting gains (calculated in Apper (67)m= 53.52 47.53 38.66 29 Appliances gains (calculated in Apper (68)m= 330.99 334.43 325.77 30 | 43.93 Apr May 9.03 149.03 Apr May 9.03 Apr May | 38.47 Vinder is Jun 149.03 Dn L9 or 18.47 ation L1 262.23 | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Tal 252.84 | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 | 50.76 om com Nov 149.03 | 54.85 munity h | | (66) |
| (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (6 5. Internal gains (see Table 5 and Metabolic gains (Table 5), Watts Jan Feb Mar A (66)m= 149.03 149.03 149.03 14 Lighting gains (calculated in Apper (67)m= 53.52 47.53 38.66 29 Appliances gains (calculated in Apper (68)m= 330.99 334.43 325.77 30 Cooking gains (calculated in Apper (68)m= 330.99 334.43 325.77 30 | Apr May 9.03 149.03 149.03 149.03 21.88 pendix L, equation 7.35 284.09 ndix L, equation 7.35 284.09 | 38.47 Jun 149.03 on L9 or 18.47 ation L1 262.23 on L15 or | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 , also se | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Tall 252.84 ee Table | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 | 50.76 om com Nov 149.03 51.6 | 54.85 munity h Dec 149.03 55 316.39 | | (66) (67) (68) |
| (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (6 5. Internal gains (see Table 5 and Metabolic gains (Table 5), Watts Jan Feb Mar A (66)m= 149.03 149.03 149.03 14 Lighting gains (calculated in Apper (67)m= 53.52 47.53 38.66 29 Appliances gains (calculated in Apper (68)m= 330.99 334.43 325.77 30 Cooking gains (calculated in Apper (69)m= 52.39 52.39 52.39 52.39 52.39 | 43.93 Apr May 9.03 149.03 Apr May 9.03 Apr May | 38.47 Vinder is Jun 149.03 Dn L9 or 18.47 ation L1 262.23 | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Tal 252.84 | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 | 50.76 om com Nov 149.03 | 54.85 munity h Dec 149.03 | | (66) (67) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculate 5 and (66)m in calculate 6 and (66)m i | Apr May 9.03 149.03 149.03 149.03 126 21.88 1284.09 12.39 52.39 | 38.47 Ilinder is Jun 149.03 On L9 or 18.47 ation L1 262.23 on L15 or 52.39 | Jul 149.03 L9a), a 19.96 13 or L13 247.62 or L15a) 52.39 | Aug 149.03 Iso see 25.94 3a), also 244.19 a, also se 52.39 | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Tal 252.84 ee Table 52.39 | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 52.39 | 50.76 om com Nov 149.03 51.6 294.53 | 54.85 munity h Dec 149.03 55 316.39 | | (66) (67) (68) (69) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculate 5 and (66)m in calculate 5 and (68)m in calculate 6 and (68)m i | Apr May 9.03 149.03 149.03 149.03 126 21.88 129.03 284.09 100.26 239 52.39 3 | 38.47 Ilinder is Jun 149.03 on L9 or 18.47 ation L1 262.23 on L15 or 52.39 | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 , also se | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Tall 252.84 ee Table | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 | 50.76 om com Nov 149.03 51.6 | 54.85 munity h Dec 149.03 55 316.39 | | (66) (67) (68) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculated 53 and Metabolic gains (Table 5), Watts Jan | 43.93 43.93 65)m only if cy d 5a): Apr May 9.03 14 | 38.47 Vinder is Jun 149.03 on L9 or 18.47 ation L1 262.23 on L15 or 52.39 3 e 5) | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 , also se 52.39 | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Tall 252.84 ee Table 52.39 | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 52.39 | 50.76 om com Nov 149.03 51.6 294.53 52.39 | 54.85 munity h Dec 149.03 55 316.39 52.39 | | (66) (67) (68) (69) (70) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculated 5 and Metabolic gains (Table 5), Watts Jan | Apr May 9.03 149.03 149.03 149.03 126 21.88 129.03 284.09 100.26 239 52.39 3 | 38.47 Ilinder is Jun 149.03 on L9 or 18.47 ation L1 262.23 on L15 or 52.39 | Jul 149.03 L9a), a 19.96 13 or L13 247.62 or L15a) 52.39 | Aug 149.03 Iso see 25.94 3a), also 244.19 a, also se 52.39 | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Tal 252.84 ee Table 52.39 | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 52.39 | 50.76 om com Nov 149.03 51.6 294.53 | 54.85 munity h Dec 149.03 55 316.39 | | (66) (67) (68) (69) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculated 5 and Metabolic gains (Table 5), Watts Jan | Apr May 9.03 149.03 149.03 149.03 149.03 126 21.88 1284.09 128.39 52.39 13 3 3 3 4 4 1 4 1 4 1 4 1 4 1 4 1 4 1 | 38.47 Ilinder is Jun 149.03 On L9 or 18.47 ation L1 262.23 on L15 or 52.39 3 e 5) -99.35 | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 , also se 52.39 3 | 41.02 or hot was Sep 149.03 Table 5 34.82 o see Talle 252.84 ee Table 52.39 | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 52.39 3 | 50.76 om com Nov 149.03 51.6 294.53 52.39 3 | 54.85 munity h Dec 149.03 55 316.39 52.39 3 | | (66) (67) (68) (69) (70) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculated 53 and in calculated 54 and in calculated 55 and in calculated 56 and in calculated 57 in calculated 57 in calculated 58 in calculated 58 in calculated 58 in calculated 58 in calculated 59 in calc | 43.93 43.93 65)m only if cy d 5a): Apr May 9.03 14 | 38.47 Vinder is Jun 149.03 Dn L9 or 18.47 ation L1 262.23 on L15 or 52.39 3 e 5) -99.35 | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 0, also se 52.39 3 -99.35 | 41.02 or hot was seep 149.03 Table 5 34.82 o see Tall 252.84 ee Table 52.39 3 -99.35 | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 52.39 3 -99.35 | 50.76 om com Nov 149.03 51.6 294.53 52.39 3 -99.35 | 54.85 munity h Dec 149.03 55 316.39 52.39 3 -99.35 | | (66) (67) (68) (69) (70) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculated 53 and in calculated 54 and in calculated 55 and in calculated 56 and in calculated | Apr May 9.03 149 | 38.47 Ilinder is Jun 149.03 On L9 or 18.47 ation L1 262.23 on L15 or 52.39 3 e 5) -99.35 | 36.21 Jul 149.03 L9a), a 19.96 13 or L13 247.62 or L15a) 52.39 3 -99.35 48.67 m + (67)m | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 a), also se 52.39 3 -99.35 | 41.02 or hot was seep 149.03 Table 5 34.82 see Table 52.39 3 -99.35 56.97 + (69)m + (| 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 52.39 3 -99.35 63.32 70)m + (7 | 50.76 om com Nov 149.03 51.6 294.53 52.39 3 -99.35 70.5 1)m + (72) | 54.85 munity h Dec 149.03 55 316.39 52.39 3 -99.35 73.73 | | (66) (67) (68) (69) (70) (71) |
| include (57)m in calculation of (65)m= 56.46 49.53 51.47 45 include (57)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculation of (65)m in calculated 53 and in calculated 54 and in calculated 55 and in calculated 56 and in calculated 57 and in calculated 57 and in calculated 58 and in calculated 58 and in calculated 58 and in calculated 58 and in calculated 59 and in calc | Apr May 9.03 149 | 38.47 Vinder is Jun 149.03 Dn L9 or 18.47 ation L1 262.23 on L15 or 52.39 3 e 5) -99.35 | 36.21 S in the control of the contr | 40.76 dwelling Aug 149.03 lso see 25.94 3a), also 244.19 0, also se 52.39 3 -99.35 | 41.02 or hot was seep 149.03 Table 5 34.82 o see Tall 252.84 ee Table 52.39 3 -99.35 | 47.11 ater is fr Oct 149.03 44.21 ble 5 271.27 5 52.39 3 -99.35 | 50.76 om com Nov 149.03 51.6 294.53 52.39 3 -99.35 | 54.85 munity h Dec 149.03 55 316.39 52.39 3 -99.35 | | (66) (67) (68) (69) (70) |

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.



| Orientation: | Access F Table 6d | actor | Area m² | | | Flu: Tab | x ole 6a | | 9_ Table | e 6b | | FF Table 6c | | Gains (W) | |
|--------------------------|----------------------|------------|------------|----------|---------------|-------------|-------------|--------|--|-------|--------|----------------|----------|--------------|------|
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | x | 1 | 1.28 | x | 0.6 | 3 | x | 0.7 | = | 13.07 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 2 | 2.97 | X | 0.6 | 3 | x | 0.7 | = | 26.6 | (75) |
| Northeast 0.9x | 0.77 | X | 3.7 | 9 | x | 4 | 1.38 | X | 0.6 | 3 | x | 0.7 | = | 47.93 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 6 | 7.96 | X | 0.6 | 3 | x | 0.7 | = | 78.71 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 9 | 1.35 | X | 0.6 | 3 | x | 0.7 | = | 105.8 | (75) |
| Northeast 0.9x | 0.77 | X | 3.7 | 9 | X | 9 | 7.38 | X | 0.6 | 3 | x | 0.7 | = | 112.8 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 9 | 91.1 | X | 0.6 | 3 | x | 0.7 | = | 105.52 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 7. | 2.63 | X | 0.6 | 3 | x | 0.7 | = | 84.12 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 5 | 0.42 | X | 0.6 | 3 | x | 0.7 | = | 58.4 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 2 | 8.07 | X | 0.6 | 3 | x | 0.7 | = | 32.51 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 1 | 4.2 | X | 0.6 | 3 | x | 0.7 | = | 16.44 | (75) |
| Northeast 0.9 | 0.77 | X | 3.7 | 9 | X | 9 |).21 | X | 0.6 | 3 | x | 0.7 | = | 10.67 | (75) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 3 | 6.79 |] | 0.6 | 3 | x | 0.7 | = | 79.84 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 6 | 2.67 |] | 0.6 | 3 | x | 0.7 | = | 135.99 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 8 | 5.75 | | 0.6 | 3 | x | 0.7 | = | 186.07 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 10 | 06.25 |] | 0.6 | 3 | x | 0.7 | = | 230.55 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 11 | 19.01 |] | 0.6 | 3 | x | 0.7 | = | 258.24 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 11 | 18.15 | | 0.6 | 3 | x | 0.7 | = | 256.37 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | x | 11 | 13.91 |] | 0.6 | 3 | x | 0.7 | = | 247.17 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 10 |)4.39 |] | 0.6 | 3 | x | 0.7 | = | 226.51 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 9 | 2.85 |] | 0.6 | 3 | x | 0.7 | = | 201.47 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | x | 6 | 9.27 |] | 0.6 | 3 | x | 0.7 | = | 150.3 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 4 | 4.07 |] | 0.6 | 3 | x | 0.7 | = | 95.63 | (79) |
| Southwest _{0.9} | 0.77 | X | 7. | 1 | X | 3 | 1.49 |] | 0.6 | 3 | x | 0.7 | = | 68.32 | (79) |
| Solar gains i | n watte ca | olculated | for each | n month | • | | | (83)n | n = Sum(7 | 74.)m | (82)m | | | | |
| (83)m= 92.91 | 1 1 | 234 | 309.26 | 364.04 | $\overline{}$ | 69.17 | 352.69 | 310 | | 9.88 | 182.81 | 112.07 | 79 | 1 | (83) |
| Total gains - | internal a | nd solar | (84)m = | (73)m | + (8 | 33)m , | watts | | | | | 1 | <u> </u> | _ | |
| (84)m= 658.3 | 6 723.33 | 772.67 | 813.97 | 834.11 | 80 | 08.35 | 774 | 740 | .61 70 | 9.56 | 666.67 | 633.76 | 629.18 |] | (84) |
| 7. Mean int | ernal temp | erature | (heating | seasor | า) | | | | | | | • | | _ | |
| Temperatur | | | | | | area f | rom Tal | ble 9 | , Th1 (° | C) | | | | 21 | (85) |
| Utilisation fa | actor for ga | ains for I | iving are | a, h1,n | - 1 (se | ee Ta | ble 9a) | | | | | | | | |
| Jan | Feb | Mar | Apr | May | Ì | Jun | Jul | Α | ug S | Sep | Oct | Nov | Dec |] | |
| (86)m= 0.97 | 0.96 | 0.93 | 0.88 | 0.78 | (| 0.63 | 0.49 | 0.9 | 53 0. | 73 | 0.89 | 0.95 | 0.97 | 1 | (86) |
| Mean interr | nal tempera | ature in I | iving are | ea T1 (f | ollo | w stei | os 3 to 7 | 7 in 1 | able 9d | :) | | • | | _ | |
| (87)m= 19.81 | | 20.17 | 20.45 | 20.69 | _ | 0.84 | 20.9 | 20. | | .79 | 20.49 | 20.11 | 19.79 |] | (87) |
| Temperatur | e during h | eating p | eriods ir | rest of | dw | elling | from Ta | able | 9, Th2 (| °C) | | | | _ | |
| (88)m= 19.98 | | 19.99 | 19.99 | 19.99 | _ | 9.99 | 19.99 | 19. | ` | .99 | 19.99 | 19.99 | 19.99 | | (88) |
| Utilisation fa | actor for a | ains for r | est of d | welling | h2 | m (se | e Table | 9a) | | | | • | | - | |
| (89)m= 0.96 | | 0.92 | 0.85 | 0.74 | _ | 0.56 | 0.39 | 0.4 | 12 0. | 66 | 0.86 | 0.94 | 0.97 | 7 | (89) |
| | | | | <u> </u> | | ! | | | | ! | | | <u> </u> | _ | |



| 0)m= | 18.4 | 18.6 | 18.92 | 19.32 | 19.64 | 19.82 | 19.87 | 19.86 | 7 in Tabl _{19.76} | 19.38 | 18.84 | 18.38 | | (90 |
|---|--|--|--|---|--|----------------------------|----------------------|--|---|----------------------------------|--|------------------------|-----------------------------------|--|
| 0)m= | 10.4 | 10.0 | 10.92 | 19.32 | 19.04 | 19.02 | 19.07 | 19.00 | | | 10.04 g area ÷ (4 | | 0.04 | ` |
| | | | | | | | | | ' | LA - LIVIII | g area · (- | ', - | 0.24 | (91 |
| Mear | interna | temper | ature (fo | r the wh | ole dwe | lling) = fl | LA × T1 | + (1 – fL | A) × T2 | | | | | |
| 2)m= | 18.74 | 18.93 | 19.23 | 19.59 | 19.89 | 20.07 | 20.12 | 20.11 | 20.01 | 19.65 | 19.15 | 18.72 | | (92 |
| Apply | / adjustn | nent to tl | ne mean | internal | tempera | ature fro | m Table | 4e, whe | ere appro | priate | | | | |
| 3)m= | 18.59 | 18.78 | 19.08 | 19.44 | 19.74 | 19.92 | 19.97 | 19.96 | 19.86 | 19.5 | 19 | 18.57 | | (9 |
| 3. Sp | ace hea | ting requ | uirement | | | | | | | | | | | |
| | | | ernal ten or gains ι | • | | ed at ste | ep 11 of | Table 9l | b, so tha | t Ti,m=(7 | 76)m and | d re-calc | ulate | |
| | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | | |
| Jtilis | ation fac | tor for g | ains, hm | : | | • | • | • | • | | | | | |
| l)m= | 0.95 | 0.94 | 0.9 | 0.84 | 0.72 | 0.55 | 0.38 | 0.42 | 0.65 | 0.85 | 0.93 | 0.96 | | (9 |
| Jsef | ul gains, | hmGm . | W = (94 | l)m x (84 | 4)m | | | | | | | | | |
| 5)m= | 627.79 | 676.56 | 697.16 | 680.93 | 602.73 | 445.45 | 296.73 | 311.41 | 458.66 | 564.29 | 589.87 | 603.45 | | (9 |
| 1ont | hly avera | age exte | rnal tem | perature | from Ta | able 8 | ! | | ! | | | | | |
| 8)m= | 4.3 | 4.9 | 6.5 | 8.9 | 11.7 | 14.6 | 16.6 | 16.4 | 14.1 | 10.6 | 7.1 | 4.2 | | (9 |
| leat | loss rate | for mea | an intern | al tempe | erature, l | Lm , W = | =[(39)m : | x [(93)m | – (96)m | 1 | | | | |
| ')m= | 1306.82 | | 1141.28 | 949.31 | 724.07 | 478.68 | 303.38 | 320.86 | 518.77 | 801.44 | 1071.32 | 1293.95 | | (9 |
| bac | e heatin | a reauire | ement for | r each m | nonth. k\ | ı Nh/mont | th = 0.02 | 24 x [(97 |)m – (95 |)m] x (41 | 1)m | | | |
| 3)m= | 505.2 | 395.03 | 330.42 | 193.23 | 90.27 | 0 | 0 | 0 | 0 | 176.44 | 346.64 | 513.73 | | |
| ′ | | | | | | · · | l ' | | | - | | | | |
| | | | | | | | • | Tota | l ner vear | /k\Wh/year |) = Sum(9) | 8), 50 40 = | 2550.96 | (9 |
| | | | | | | | | Tota | l per year | (kWh/year |) = Sum(9 | 8) _{15,912} = | 2550.96 | = |
| Spac | e heatin | g require | ement in | kWh/m² | /year | | | Tota | l per year | (kWh/year |) = Sum(9 | 8) _{15,912} = | 2550.96 31.45 | = |
| | | • • | ement in nts – Indi | | | ystems i | ncluding | | | (kWh/year |) = Sum(9 | 8) _{15,912} = | | (9 (9 |
| ı. Er | | uiremer | | | | ystems i | ncluding | | | (kWh/year |) = Sum(9 | 8) _{15,912} = | | = |
| . Er Spac | ergy rec | uiremer ng: | | vidual h | eating sy | | | ı micro-C | | kWh/year |) = Sum(9 | 8) _{15,912} = | | (9 |
| . Er Spac | ergy receive heating ion of sp | uiremer ng: pace hea | nts – Indi | vidual ho | eating sy | | system | ı micro-C | CHP) | kWh/year |) = Sum(9 | 8) _{15,912} = | 31.45 | (9 |
| i. Er pac ract | ergy receive heating ion of spanson ion of spanson ion of spanson ion of spanson ion ion ion ion ion ion ion ion ion i | uiremer ig: bace hea bace hea | nts – Indi nt from se nt from m | vidual he econdary ain syst | eating sy y/supple em(s) | | system | (202) = 1 | CHP) | |) = Sum(9 | 8)15,912 = | 31.45 0 1 | (9) |
| pac Fract Fract | ergy receive heating ion of spanion of to | uiremer ng: pace hea pace hea tal heatin | nts - Indi nt from se nt from m | vidual he econdary ain syst main sys | eating sy y/supple em(s) stem 1 | | system | (202) = 1 | CHP) - (201) = | |) = Sum(9 | 8) _{15,912} = | 0 1 1 | (9) |
| pactractractract | ergy receive heating ion of spinon of to ency of receivers | uiremen ng: pace hea pace hea tal heatii main spa | nts – Indi at from se at from m ag from r ace heati | vidual ho econdary ain syst main sys ng syste | eating sy y/supple em(s) stem 1 | mentary | system | (202) = 1 | CHP) - (201) = | |) = Sum(9 | 8)15,912 = | 31.45 0 1 1 90.2 | (9) |
| pactractract | ergy receive heating ion of spinon of to ency of receivers | uiremen ng: pace hea pace hea tal heatii main spa | nts - Indi nt from se nt from m | vidual ho econdary ain syst main sys ng syste | eating sy y/supple em(s) stem 1 | mentary | system | (202) = 1 | CHP) - (201) = | |) = Sum(9 | 8) _{15,912} = | 0 1 1 | (9) |
| Er pac ract ract ract | ergy receive heating ion of spinon of to ency of receivers | uiremen ng: pace hea pace hea tal heatii main spa | nts – Indi at from se at from m ag from r ace heati | vidual ho econdary ain syst main sys ng syste | eating sy y/supple em(s) stem 1 | mentary | system | (202) = 1 | CHP) - (201) = | |) = Sum(9: | 8) _{15,912} = | 31.45 0 1 1 90.2 | (9) |
| Eract Fract Fract Fract Fract | ergy receive heating ion of spinon of to ency of rency of spinon o | uiremenng: pace head pace head tal heating main space seconda | at from set that from many from reace heating | vidual he econdary ain syst main syst ng syste ementary | eating sy y/supple em(s) stem 1 em 1 y heating | mentary g system Jun | system | micro-C (202) = 1 (204) = (2 | CHP) - (201) = 02) × [1 - (| [203)] = | | | 0 1 1 90.2 | (9) |
| Eract Fract Fract Fract Effici | ergy receive heating ion of spinon of to ency of rency of spinon o | uiremenng: pace head pace head tal heating main space seconda | nts – Indi nt from se nt from m ng from r ace heati ry/supple Mar | vidual he econdary ain syst main syst ng syste ementary | eating sy y/supple em(s) stem 1 em 1 y heating | mentary g system Jun | system | micro-C (202) = 1 (204) = (2 | CHP) - (201) = 02) × [1 - (| [203)] = | | | 0 1 1 90.2 | (9) |
| . Er Fract Fract Fract Fract Effici | ergy receive heating ion of spinor of to ency of spinor | uiremer ng: nace hea nace hea tal heatii main spa seconda Feb g require 395.03 | at from set from many from reace heating the many from the | econdary ain systemain systemain systementary Apralculated | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 | mentary g system Jun | system 1, % Jul | micro-C (202) = 1 - (204) = (2 | CHP) - (201) = 02) × [1 - (| (203)] = | Nov | Dec | 0 1 1 90.2 | (9) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2 |
| . Er Fract Fract Fract Fract Effici | ergy receive heating ion of spinor of to ency of spinor | uiremen ng: pace hea tal heatin main spa seconda Feb g require 395.03 | at from set from many from reace heating from Mar Mar (c. 330.42 4)] } x 1 | econdary ain systemain systemain systementary Apr Alculated 193.23 | eating sylvasple em(s) stem 1 em 1 May dabove; 90.27 | mentary g system Jun 0 | system 1, % Jul 0 | micro-C (202) = 1 · (204) = (2 | CHP) - (201) = 02) × [1 - 0 | Oct 176.44 | Nov 346.64 | Dec 513.73 | 0 1 1 90.2 | (9) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2 |
| n. Er Fract Fract Fract Fract Effici | ergy receive heating ion of spinon of to ency of receive heating to be seen t | uiremer ng: nace hea nace hea tal heatii main spa seconda Feb g require 395.03 | at from set from many from reace heating the many from the | econdary ain systemain systemain systementary Apralculated | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 | mentary g system Jun | system 1, % Jul | micro-C (202) = 1 · (204) = (2 Aug 0 | CHP) - (201) = 02) × [1 - (| Oct 176.44 195.61 | Nov 346.64 384.3 | Dec 513.73 | 0 1 1 90.2 0 kWh/y | (9 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 |
| a. Er Spac Fract Fract Effici Spac 11)r | ergy receive heating ion of sprion of to ency of security of security in the s | uiremenng: pace head tal heating main space seconda Feb g require 395.03)m x (20 437.94 | at from set from many from race heating from the ment (co. 330.42 4)] } x 1 | econdary ain systemain systemain systementary Apralculated 193.23 00 ÷ (20 214.22 | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 e6) 100.08 | mentary g system Jun 0 | system 1, % Jul 0 | micro-C (202) = 1 · (204) = (2 Aug 0 | CHP) - (201) = 02) × [1 - 0 | Oct 176.44 195.61 | Nov 346.64 384.3 | Dec 513.73 | 0 1 1 90.2 | (9) (9) (9) (9) (9) (9) (9) (9) (9) (9) |
| a. Er Fract Fract Effici Effici | ergy receive heating ion of spinon of to ency of security and ency of se | uiremer ng: pace hea pace hea tal heatin main spa seconda Feb g require 395.03)m x (20 437.94 | ats – Indirect from set from many from ment (call 330.42 d)] } x 1 366.32 | econdary ain systemain systemain systementary Apralculated 193.23 00 ÷ (20 214.22 | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 e6) 100.08 | mentary g system Jun 0 | system 1, % Jul 0 | micro-C (202) = 1 · (204) = (2 Aug 0 | CHP) - (201) = 02) × [1 - (| Oct 176.44 195.61 | Nov 346.64 384.3 | Dec 513.73 | 0 1 1 90.2 0 kWh/y | (9) (9) (9) (9) (9) (9) (9) (9) (9) (9) |
| a. Er Fract Fract Fract Effici Effici | ergy receive heating ion of sprion of to ency of receive heating to the sprion of the spring of the sprion of the | uirements ng: pace heater pace heater tal heatin main space seconda Feb g require 395.03)m x (20 437.94 g fuel (second) } x 1 | t from set t from many fro | econdary ain systemain systemain systematary Apralculated 193.23 00 ÷ (20 214.22 | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 e6) 100.08 | g system Jun 0 | system 1, % Jul 0 | micro-C (202) = 1 - (204) = (2 Aug 0 Tota | Sep 0 0 0 0 0 0 0 0 0 0 0 0 0 | Oct 176.44 195.61 ir) = Sum(2 | Nov 346.64 384.3 211) _{15,1012} | Dec 513.73 569.55 | 0 1 1 90.2 0 kWh/y | (9) (9) (9) (9) (9) (9) (9) (9) (9) (9) |
| a. Er Fract Fract Fract Effici Effici | ergy receive heating ion of sprion of to ency of receive heating to the sprion of the spring of the sprion of the | uiremer ng: pace hea pace hea tal heatin main spa seconda Feb g require 395.03)m x (20 437.94 | ats – Indirect from set from many from ment (call 330.42 d)] } x 1 366.32 | econdary ain systemain systemain systementary Apralculated 193.23 00 ÷ (20 214.22 | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 e6) 100.08 | mentary g system Jun 0 | system 1, % Jul 0 | micro-C (202) = 1 · (204) = (2 Aug 0 Tota | CHP) - (201) = 02) × [1 - (1) Sep 0 0 0 I (kWh/yea | Oct 176.44 195.61 Ir) = Sum(2 | Nov 346.64 384.3 211) _{15,1012} | Dec 513.73 569.55 | 0 1 1 90.2 0 kWh/y | (9 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 (2 |
| a. Er Space Fract Fract Effici Effici 11)r | ergy receive heating ion of sprion of to ency of receive heating to the sprion of the spring of the sprion of the | uirements ng: pace heater pace heater tal heatin main space seconda Feb g require 395.03)m x (20 437.94 g fuel (second) } x 1 | t from set t from many fro | econdary ain systemain systemain systematary Apralculated 193.23 00 ÷ (20 214.22 | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 e6) 100.08 | g system Jun 0 | system 1, % Jul 0 | micro-C (202) = 1 · (204) = (2 Aug 0 Tota | Sep 0 0 0 0 0 0 0 0 0 0 0 0 0 | Oct 176.44 195.61 Ir) = Sum(2 | Nov 346.64 384.3 211) _{15,1012} | Dec 513.73 569.55 | 0 1 1 90.2 0 kWh/y | (g) |
| a. Er Fract Fract Fract Effici Space 11)r | ergy receive heating ion of sprion of to ency of receive heating to the sprion of the spring of the sprion of the | uiremen ng: pace hea pace hea tal heatin main spa seconda Feb g require 395.03)m x (20 437.94 g fuel (second) 0 | t from set t from many fro | econdary ain systemain systemain systematary Apralculated 193.23 00 ÷ (20 214.22 | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 e6) 100.08 | g system Jun 0 | system 1, % Jul 0 | micro-C (202) = 1 · (204) = (2 Aug 0 Tota | CHP) - (201) = 02) × [1 - (1) Sep 0 0 0 I (kWh/yea | Oct 176.44 195.61 Ir) = Sum(2 | Nov 346.64 384.3 211) _{15,1012} | Dec 513.73 569.55 | 0 1 1 90.2 0 kWh/y | (g) |
| a. Er Fract Fract Fract Effici Effici 11)r Spac ([(98 | ergy receive heating ion of spinon of to ency of receive heating 505.2 n = {[(98 560.09)] heating trom with the from with the ency of th | uirements ng: pace heater pace heater heater heater uirements pace heater pa | trom set trom many from race heating ry/supplement (calculater (ca | econdary ain systemain systemain systementary Apr alculated 193.23 00 ÷ (20 214.22 y), kWh/ 8) 0 | eating sylvasple em(s) stem 1 em 1 y heating May d above; 90.27 e6) 100.08 month | g system Jun 0 | system n, % Jul 0 | micro-C (202) = 1 · (204) = (2 Aug 0 Tota | CHP) - (201) = 02) × [1 - (1) Sep 0 0 I (kWh/yea | Oct 176.44 195.61 Ir) =Sum(2 | Nov 346.64 384.3 211) _{15,1012} 0 215) _{15,1012} | Dec 513.73 569.55 | 0 1 1 90.2 0 kWh/y | (9) |
| a. Er Fract Fract Effici Effici 11)r Space ([(98 | ergy receive heating ion of spinon of to ency of receive heating 505.2 an = {[(98) 560.09]} e heating ion x (20) 100 100 100 100 100 100 100 100 100 1 | uirement of the property of th | t from set from many from reace heating from the ment (call 330.42 4)] } x 1 366.32 econdary 00 ÷ (200 0 | econdary ain systemain systematary Apr alculated 193.23 00 ÷ (20 214.22 y), kWh/ 8) 0 | eating sylvasple em(s) stem 1 em 1 y heating May d above 90.27 e6) 100.08 | g system Jun 0 | system 1, % Jul 0 | micro-C (202) = 1 · (204) = (2 Aug 0 Tota | CHP) - (201) = 02) × [1 - (1) Sep 0 0 0 I (kWh/yea | Oct 176.44 195.61 Ir) = Sum(2 | Nov 346.64 384.3 211) _{15,1012} | Dec 513.73 569.55 | 0 1 1 90.2 0 kWh/y | (g) |



| | | | | | | | | | | _ | |
|--|-------------|-------------|-------------------|----------------------|------------|-----------|-----------------------|---------|-------------------|---------------------|--------------|
| (217)m= 89.43 89.37 89.23 | 88.95 | 88.43 | 87.3 | 87.3 | 87.3 | 87.3 | 88.86 | 89.27 | 89.46 | | (217) |
| Fuel for water heating, kWh/r $(219)m = (64)m \times 100 \div (21)m$ | | | | | | | | | | | |
| (219)m= 196.43 172.61 179.99 | | 155.88 | 138.83 | 131.24 | 146.95 | 147.64 | 165.96 | 177.34 | 190.96 |] | |
| | | | | | Tota | I = Sum(2 | 19a) ₁₁₂ = | | | 1963.57 | (219) |
| Annual totals | | 4 | | | | | k' | Wh/yea | r | kWh/year | 7 |
| Space heating fuel used, mai | n system | I | | | | | | | | 2828.11 | <u> </u> |
| Water heating fuel used Electricity for pumps, fans an | d electric | keen ho | + | | | | | | | 1963.57 | J |
| mechanical ventilation - bala | | · | | anut fron | n outside | a | | | 60.52 | 1 | (230a) |
| | iriceu, exi | ii act or p | ositive ii | iput iioi | ii outside | - | | | |]] | |
| central heating pump: | _ | | | | | | | | 30 |] | (230c) |
| boiler with a fan-assisted flu | | | | | | -f (220-) | (220-1) - | | 45 |] | (230e) |
| Total electricity for the above | kwn/yea | ır | | | sum | or (230a) | (230g) = | | | 135.52 | (231) |
| Electricity for lighting | | | | | | | | | | 378.04 | (232) |
| Electricity generated by PVs | | | | | | | | | | -602.4 | (233) |
| 10a. Fuel costs - individual h | eating sy | stems: | | | | | | | | | |
| | | | Fu kW | el /h/year | | | Fuel P (Table | | | Fuel Cost £/year | |
| Space heating - main system | 1 | | (21 | 1) x | | | 3.4 | -8 | x 0.01 = | 98.42 | (240) |
| Space heating - main system | 2 | | (213 | 3) x | | | 0 | | x 0.01 = | 0 | (241) |
| Space heating - secondary | | | (21 | 5) x | | | 13. | 19 | x 0.01 = | 0 | (242) |
| Water heating cost (other fue | l) | | (219 | 9) | | | 3.4 | -8 | x 0.01 = | 68.33 | (247) |
| Pumps, fans and electric kee | p-hot | | (23 | 1) | | | 13. | 19 | x 0.01 = | 17.88 | (249) |
| (if off-peak tariff, list each of (Energy for lighting | 230a) to (| (230g) s | eparately (232 | | licable a | nd apply | fuel pri | | rding to x 0.01 = | Table 12a 49.86 | (250) |
| Additional standing charges (| Table 12) | | | | | | | | | 120 | (251) |
| | | | one | of (233) to | o (235) x) | | 13. | 19 | x 0.01 = | -79.46 |] (252) |
| Appendix Q items: repeat line | es (253) a | nd (254) | as need | ded | | | 10. | | | 10.10 | J\ ' ' / |
| Total energy cost | (_00) a | ` ′ | (247) + (25 | | = | | | | | 275.03 | (255) |
| 11a. SAP rating - individual | neating sy | ystems | | | | | | | | | |
| Energy cost deflator (Table 1 | 2) | | | | | | | | | 0.42 | (256) |
| Energy cost factor (ECF) | , | [(255) x | : (256)] ÷ [(| (4) + 45.0] | = | | | | | 0.92 | (257) |
| SAP rating (Section 12) | | | | | | | | | | 87.22 | (258) |
| 12a. CO2 emissions – Indivi | dual heat | ing syste | ems inclu | uding mi | cro-CHF |) | | | | | _ |
| | | | En | ergy | | | Fmice | ion fac | tor | Emissions | |
| | | | | /h/year | | | kg CO | | W | kg CO2/yea | ır |
| Space heating (main system | 1) | | (21 | 1) x | | | 0.2 | 16 | = | 610.87 | (261) |



| Space heating (secondary) | (215) x | 0.519 | 0 (263) |
|---|---------------------------------|-----------------|---------------|
| Water heating | (219) x | 0.216 | 424.13 (264) |
| Space and water heating | (261) + (262) + (263) + (264) = | | 1035 (265) |
| Electricity for pumps, fans and electric keep-hot | (231) x | 0.519 | 70.34 (267) |
| Electricity for lighting | (232) x | 0.519 | 196.2 (268) |
| Energy saving/generation technologies | | | |
| Item 1 | | 0.519 | -312.64 (269) |
| Total CO2, kg/year | sum | of (265)(271) = | 988.9 (272) |
| CO2 emissions per m ² | (272 | ?) ÷ (4) = | 12.19 (273) |
| El rating (section 14) | | | 89 (274) |

13a. Primary Energy

| | Energy kWh/year | Primary factor | P. Energy kWh/year |
|---|---------------------------------|-----------------------|------------------------------|
| Space heating (main system 1) | (211) x | 1.22 | 3450.3 (261) |
| Space heating (secondary) | (215) x | 3.07 | 0 (263) |
| Energy for water heating | (219) x | 1.22 | 2395.55 (264) |
| Space and water heating | (261) + (262) + (263) + (264) = | | 5845.85 (265) |
| Electricity for pumps, fans and electric keep-hot | (231) x | 3.07 | 416.06 (267) |
| Electricity for lighting | (232) x | 0 = | 1160.58 (268) |
| Energy saving/generation technologies | | | |
| Item 1 | | 3.07 | -1849.36 (269) |
| 'Total Primary Energy | sum | of (265)(271) = | 5573.12 (272) |
| Primary energy kWh/m²/year | (272 |) ÷ (4) = | 68.7 (273) |

SAP 2012 Overheating Assessment



Calculated by Stroma FSAP 2012 program, produced and printed on 17 December 2019

Property Details: 10-17-65487 Plot 25 (Type B)

Dwelling type: Semi-detached House

Located in: **England** Region: East Anglia **Cross ventilation possible:** Yes

Number of storeys: 2

Front of dwelling faces: North East

Overshading: Average or unknown

Overhangs: None

Thermal mass parameter: Calculated 153.58

Night ventilation: False

Blinds, curtains, shutters:

Ventilation rate during hot weather (ach): 4 (Windows open half the time)

Overheating Details:

Summer ventilation heat loss coefficient: (P1) 273.05

Transmission heat loss coefficient: 55.9

Summer heat loss coefficient: 328.95 (P2)

Overhangs:

Orientation: Ratio: **Z_overhangs:**

0 North East (Front) 1 South West (Rear) 0 1

Solar shading:

Solar gains:

| Orientation: | Z biinas: | Solar access: | Overnangs: | Z summer: | |
|--------------------|-----------|---------------|------------|-----------|------|
| North East (Front) | 1 | 0.9 | 1 | 0.9 | (P8) |
| South West (Rear) | 1 | 0.9 | 1 | 0.9 | (P8) |

South West (Rear) 0.9 1 0.9 1

Orientation FF Flux **Shading** Gains Area g_ North East (Front) 0.9 x 3.79 100.04 0.63 0.7 0.9 135.44 South West (Rear) 0.9 x7.1 122.31 0.7 0.9 310.21 0.63 **Total** 445.65 (P3/P4)

Internal gains:

| | June | July | August | |
|--|-----------------|--------|--------|------|
| Internal gains | 436.19 | 418.31 | 426.97 | |
| Total summer gains | 907.46 | 863.97 | 821.91 | (P5) |
| Summer gain/loss ratio | 2.76 | 2.63 | 2.5 | (P6) |
| Mean summer external temperature (East Anglia) | 15.4 | 17.6 | 17.6 | |
| Thermal mass temperature increment | 0.92 | 0.92 | 0.92 | |
| Threshold temperature | 19.08 | 21.15 | 21.02 | (P7) |
| Likelihood of high internal temperature | Not significant | Slight | Slight | |

Assessment of likelihood of high internal temperature: Slight