## **Regulations Compliance Report**

Approved Document L1A, 2013 Edition, England assessed by Stroma FSAP 2012 program, Version: 1.0.5.58 *Printed on 29 November 2022 at 15:07:40* 

Project Information	on:			
Assessed By:	Liam Mason (STF	RO033679)	Building Type:	Semi-detached House
Dwelling Details:				
NEW DWELLING	DESIGN STAGE		Total Floor Area: 7	2.5m²
Site Reference :	Bell Road, Bottish	nam	Plot Reference:	Plot 33
Address :	Plot 33			
Client Details:				
Name:				
Address :				
•	s items included v te report of regula	vithin the SAP calculations. tions compliance.		
1a TER and DER				
	ing system: Mains g	as		
Fuel factor: 1.00 (r	mains gas) oxide Emission Rate	(TER)	18.54 kg/m²	
•	Dioxide Emission Ra	· · · · ·	7.57 kg/m <sup>2</sup>	ОК
1b TFEE and DF				
Target Fabric Ene	rgy Efficiency (TFE	Ξ)	49.0 kWh/m <sup>2</sup>	
Dwelling Fabric Er	nergy Efficiency (DF	EE)	44.7 kWh/m <sup>2</sup>	
2 Fabric U-value				OK
Element		Average	Highest	
External		0.19 (max. 0.30)	0.19 (max. 0.70)	ОК
Party wal	I	0.00 (max. 0.20)	-	ОК
Floor		0.11 (max. 0.25)	0.11 (max. 0.70)	OK
Roof		0.11 (max. 0.20)	0.11 (max. 0.35)	OK
Openings		1.36 (max. 2.00)	1.40 (max. 3.30)	OK
2a Thermal brid				
		rom linear thermal transmittar	ces for each junction	
3 Air permeabili			E 00 (design vol	uc)
Maximum	bility at 50 pascals		5.00 (design valı 10.0	ok OK
4 Heating efficie	encv			
Main Heatir		Database: (rev 508, produc	t index 016841):	
		Boiler systems with radiato Brand name: Vaillant Model: ecoTEC plus 824 Model qualifier: VUW GB 2 (Combi) Efficiency 89.1 % SEDBUK Minimum 88.0 %		ains gas OK
Secondary	heating system:	None		

# **Regulations Compliance Report**

Hot water Storage:	No cylinder		
ontrols			
Space heating controls	TTZC by plumbing and al	actrical convices	O
Hot water controls:	TTZC by plumbing and el No cylinder thermostat		0
	No cylinder		
Boiler interlock:	Yes		OI
ow energy lights			
Percentage of fixed lights with lo	w-energy fittings	100.0%	
Minimum		75.0%	O
echanical ventilation			
Not applicable			
ummertime temperature			
Overheating risk (East Anglia):		Medium	OI
ed on:			
Overshading:		Average or unknown	
Windows facing: West		1.17m <sup>2</sup>	
Windows facing: West		1.12m <sup>2</sup>	
Windows facing: South		0.39m <sup>2</sup>	
Windows facing: East		2.98m <sup>2</sup>	
Windows facing: South		0.39m <sup>2</sup>	
Windows facing: East		1.14m <sup>2</sup>	
Windows facing: East		1.25m <sup>2</sup>	
Ventilation rate:		3.00	
Blinds/curtains:		Dark-coloured curtain or rol	ler blind
		Closed 100% of daylight ho	ours

Roofs U-value Party Walls U-value Floors U-value Photovoltaic array 0.11 W/m<sup>2</sup>K 0 W/m<sup>2</sup>K 0.11 W/m<sup>2</sup>K



Plot 33

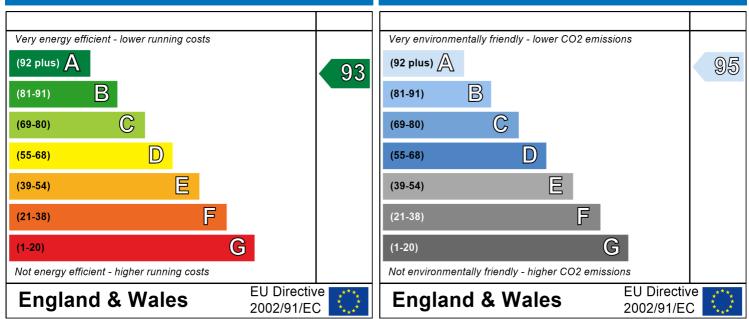
Dwelling type: Date of assessment: Produced by: Total floor area: Semi-detached House 03 November 2022 Liam Mason 72.5 m<sup>2</sup>

Environmental Impact (CO<sub>2</sub>) Rating

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2012 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO2) emissions.

#### **Energy Efficiency Rating**



The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be. The environmental impact rating is a measure of a home's impact on the environment in terms of carbon dioxide (CO2) emissions. The higher the rating the less impact it has on the environment.

# **SAP Input**

Property Details:	Plot 33					
Address:		Plot 33				
Located in:		England				
Region:		East Anglia				
UPRN:		5				
Date of assess	ment <sup>.</sup>	03 November 2022				
Date of certifie		29 November 2022				
Assessment ty		New dwelling design stage				
Transaction ty		New dwelling				
5	pe.	Unknown				
Tenure type:						
Related party		No related party				
Thermal Mass		Indicative Value Low				
	125 litres/person/da	5				
PCDF Version:		508				
Property descrip	tion:					
Dwelling type:		House				
Detachment:		Semi-detached				
Year Completed		2022				
Floor Location		Floor area:				
FIUUI LUCATION		FIOU alea.	C	torov bolabt		
			5	torey height		
Floor 0		36.25 m <sup>2</sup>		2.4 m		
Floor 1		36.25 m <sup>2</sup>		2.4 m		
Living area:		12.61 m <sup>2</sup> (fraction 0.174)				
Front of dwelling	n faces	West				
Opening types:	y 100001					
Name:	Source:	Туре:	Glazing:		Argon:	Frame:
D_1	Manufacturer	Solid	oluzing.		/ i gon.	riune.
W_1	Manufacturer	Windows	low E En - (	).05, soft coat	Yes	
	Manufacturer	Windows		0.05, soft coat	Yes	
W_2				0.05, soft coat		
W_3	Manufacturer	Windows			Yes	
W_4	Manufacturer Manufacturer	Windows		0.05, soft coat	Yes	
W_5	Manufacturor	Windows		0.05, soft coat	Yes	
W_6	Manufacturer	Windows		0.05, soft coat	Yes	
W_6 W_7		Windows Windows		0.05, soft coat	Yes Yes	
W_7 <b>Name:</b>	Manufacturer Manufacturer <b>Gap:</b>	Windows Frame Factor:	low-E, En = C	0.05, soft coat U-value:	Yes Area:	No. of Openings
W_7 <b>Name:</b> D_1	Manufacturer Manufacturer <b>Gap:</b> mm	Windows Frame Factor: 0	low-E, En = 0 <b>g-value:</b> 0	0.05, soft coat <b>U-value:</b> 1.2	Yes <b>Area:</b> 1.83	<b>No. of Openings</b> 1
W_7 <b>Name:</b> D_1 W_1	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more	Windows Frame Factor: 0 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4	Yes <b>Area:</b> 1.83 1.17	
W_7 <b>Name:</b> D_1 W_1 W_2	Manufacturer Manufacturer <b>Gap:</b> mm	Windows Frame Factor: 0	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4	Yes <b>Area:</b> 1.83 1.17 1.12	1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more 16mm or more	Windows Frame Factor: 0 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4	Yes <b>Area:</b> 1.83 1.17 1.12 0.39	1
W_7 <b>Name:</b> D_1 W_1 W_2	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more	Windows Frame Factor: 0 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4	Yes <b>Area:</b> 1.83 1.17 1.12	1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more 16mm or more	Windows Frame Factor: 0 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4	Yes <b>Area:</b> 1.83 1.17 1.12 0.39	1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4 W_5	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more 16mm or more 16mm or more	Windows <b>Frame Factor:</b> 0 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4	Yes <b>Area:</b> 1.83 1.17 1.12 0.39 2.98	1 1 1 1 1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more 16mm or more 16mm or more 16mm or more	Windows <b>Frame Factor:</b> 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63 0.63 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes <b>Area:</b> 1.83 1.17 1.12 0.39 2.98 0.39	1 1 1 1 1 1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more 16mm or more 16mm or more 16mm or more 16mm or more 16mm or more	Windows Frame Factor: 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63 0.63 0.63 0.63 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25	1 1 1 1 1 1 1 1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7 Name:	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more	Windows <b>Frame Factor:</b> 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25 Width:	1 1 1 1 1 1 1 1
W_7 Name: D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7 Name: D_1	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more	Windows Frame Factor: 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25 Width: 1.83	1 1 1 1 1 1 1 1 1 Height: 1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7 Name: D_1 W_1	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more	Windows Frame Factor: 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 Urient: West West	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25 Width: 1.83 1.17	1 1 1 1 1 1 1 1 1 Height: 1 1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7 Name: D_1 W_1 W_1 W_2	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more	Windows Frame Factor: 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 West West West West West	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25 Width: 1.83 1.17 1.12	1 1 1 1 1 1 1 1 1 1 Height: 1 1 1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7 Name: D_1 W_1 W_2 W_3	Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more	Windows Frame Factor: 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63 Vrient: West West West West South	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25 Width: 1.83 1.17 1.12 0.39	1 1 1 1 1 1 1 1 1 Height: 1 1 1 1 1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7 Name: D_1 W_1 W_2 W_3 W_4	Manufacturer Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more 16ms vindows Windows Windows Windows Windows	Windows Frame Factor: 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.64 0.65	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25 Width: 1.83 1.17 1.12 0.39 2.98	1 1 1 1 1 1 1 Height: 1 1 1 1 1 1 1 1 1 1 1 1 1
W_7 <b>Name:</b> D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7 Name: D_1 W_1 W_2 W_3 W_4 W_5 W_4 W_5 Name: D_1	Manufacturer Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or	Windows Frame Factor: 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0	low-E, En = 0 <b>g-value:</b> 0 0.63 0.64 0.65	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25 Width: 1.83 1.17 1.12 0.39 2.98 0.39	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
W_7 Name: D_1 W_1 W_2 W_3 W_4 W_5 W_6 W_7 Name: D_1 W_1 W_2 W_3 W_4	Manufacturer Manufacturer Manufacturer <b>Gap:</b> mm 16mm or more 16mm or more 16ms vindows Windows Windows Windows Windows	Windows Frame Factor: 0 0.7 0.7 0.7 0.7 0.7 0.7 0.7	low-E, En = 0 <b>g-value:</b> 0 0.63 0.64 0.65	0.05, soft coat <b>U-value:</b> 1.2 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	Yes Area: 1.83 1.17 1.12 0.39 2.98 0.39 1.14 1.25 Width: 1.83 1.17 1.12 0.39 2.98	1 1 1 1 1 1 1 Height: 1 1 1 1 1 1 1 1 1 1 1 1 1

# **SAP Input**

Overshading:		Average	e or unknown				
Opaque Elements	s:						
Туре:	Gross area:	Openings:	Net area:	U-value:	Ru value:	Curtain wall:	Kappa:
External Element							
Wall 1	84.02	10.27	73.75	0.19	0	False	N/A
Roof 1	36.25	0	36.25	0.11	0		N/A
Floor 1	36.25			0.11			N/A
Internal Element	S						
INT FLOOR	36.25						N/A
Party Elements							
Party Wall	39.42						N/A

Thermal bridges:								
Thermal bridges:	User-define	d (individual P	SI-values)	Y-Value = 0.0885				
	Length	Psi-value						
	17.06	0.16	E5	Ground floor (normal)				
	17.06	0.07	E6	Intermediate floor within a dwelling				
	9.85	0.09	E16	Corner (normal)				
	8	0.3	E2	Other lintels (including other steel lintels)				
	7.07	0.04	E3	Sill				
	17.4	0.05	E4	Jamb				
	9.06	0.06	E10	Eaves (insulation at ceiling level)				
	11.29	0.24	E12	Gable (insulation at ceiling level)				
	9.85	0.06	E18	Party wall between dwellings				
	0	0.3	E2					
	0	0.04	E3					
	0	0.05	E4					
	0	0.16	E5					
	0	0.07	E6					
	0	0.06	E10					
	0	0.24	E12					
	0	0.09	E16					
	0	-0.09	E17					
	0	0.06	E18					
	8	0.16	P1	Ground floor				
	8	0	P2	Intermediate floor within a dwelling				
	0	0.16	P1	-				
	0	0	P2					
	4.53	0.08	R4	Ridge (vaulted ceiling)				
	0	0.08	R4					
	-		-					
Ventilation:								
Pressure test:	Yes (As des	signed)						
Ventilation:		itilation (extrac	ct fans)					
Number of chimneys:	0	•						
Number of open flues:	0							
Number of fans:	2							

Pressure test:	
Main heating system:	

Number of passive stacks: Number of sides sheltered:

Main heating system:

Boiler systems with radiators or underfloor heating Gas boilers and oil boilers Fuel: mains gas Info Source: Boiler Database

2 0

2

5

# **SAP Input**

	Database: (rev 508, product index 016841) Efficiency: Winter 87.0 % Summer: 90.0 Brand name: Vaillant Model: ecoTEC plus 824 Model qualifier: VUW GB 246/5-5 (Combi boiler) Systems with radiators Central heating pump : 2013 or later Design flow temperature: Design flow temperature<=45°C Unknown Boiler interlock: Yes Delayed start
Main heating Control:	
Main heating Control:	Time and temperature zone control by suitable arrangement of plumbing and electrical services Control code: 2110
Secondary heating system:	
Secondary heating system:	None
Water heating:	
Water heating:	From main heating system Water code: 901 Fuel :mains gas No hot water cylinder Solar panel: False
Others:	
Electricity tariff: In Smoke Control Area: Conservatory: Low energy lights: Terrain type: EPC language: Wind turbine: Photovoltaics:	Standard Tariff Unknown No conservatory 100% Low rise urban / suburban English No <u>Photovoltaic 1</u> Installed Peak power: 2 Tilt of collector: 45° Overshading: None or very little Collector Orientation: East
Assess Zero Carbon Home:	No

User Details:											
Assessor Name:	Liam Masc	n			Strom	a Num	ber:		STRO	033679	
Software Name:	Stroma FS	AP 201	2		Softwa	are Vei	rsion:		Versio	on: 1.0.5.58	
			Pi	roperty	Address	: Plot 33					
Address :	Plot 33										
1. Overall dwelling dime	nsions:										
				Are	a(m²)		Av. Hei	ight(m)	-	Volume(m <sup>3</sup> )	-
Ground floor				;	36.25	(1a) x	2	4	(2a) =	87	(3a)
First floor				;	36.25	(1b) x	2	4	(2b) =	87	(3b)
Total floor area TFA = (1a	a)+(1b)+(1c)+	(1d)+(1e	e)+(1n	)	72.5	(4)			_		_
Dwelling volume						(3a)+(3b)	)+(3c)+(3d	)+(3e)+	.(3n) =	174	(5)
2. Ventilation rate:											
	main		econdar	у	other		total			m <sup>3</sup> per hour	
Number of chimneys	heating	h □_+	oeating	л + г	0	<b>Л</b> = Г	0	x 4	40 =	0	(6a)
		L +	-	」 L ヿ + ୮					20 =	-	
Number of open flues	0		0		0	」⁼∟	0			0	(6b)
Number of intermittent fa	ns						2	x ?	10 =	20	(7a)
Number of passive vents							0	х ′	10 =	0	(7b)
Number of flueless gas fi	res					Γ	0	x 4	40 =	0	(7c)
										_	-
									Air ch	anges per hou	ır
Infiltration due to chimney	-						20		÷ (5) =	0.11	(8)
If a pressurisation test has b Number of storeys in th			ed, proceed	d to (17),	otherwise	continue fr	om (9) to (	16)			
Additional infiltration	ie dweiling (n:	>)						[(0).	-1]x0.1 =	0	(9) (10)
Structural infiltration: 0.	25 for steel o	r timber t	frame or	0.35 fo	r mason	v constr	uction	[(3)	110.1 -	0	(10)
if both types of wall are pr						•				0	
deducting areas of opening	• ·				IX I						-
If suspended wooden f			ed) or 0.	1 (seal	ed), else	enter 0				0	(12)
If no draught lobby, ent Percentage of windows			rinned							0	(13)
Window infiltration	s anu uoors ui	augin si	npped		0.25 - [0.2	2 x (14) ÷ 1	001 =			0	(14) (15)
Infiltration rate							2) + (13) +	+ (15) =		0	(16)
Air permeability value,	q50, expresse	ed in cub	oic metre	s per h					area	5	(17)
If based on air permeabili	• •			•		•		•		0.36	(18)
Air permeability value applie	s if a pressurisati	on test has	s been don	e or a de	gree air pe	rmeability	is being us	sed			<b>_</b> .
Number of sides sheltere	d									2	(19)
Shelter factor					(20) = 1 -	· ·	9)] =			0.85	(20)
Infiltration rate incorporat	•				(21) = (18	) x (20) =				0.31	(21)
Infiltration rate modified for					<u> </u>	_			_	l	
	Mar Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
Monthly average wind sp			,			r	1		1	I	
(22)m= 5.1 5	4.9 4.4	4.3	3.8	3.8	3.7	4	4.3	4.5	4.7		

Wind F	actor (2	2a)m =	(22)m ÷	4										
(22a)m=	1.27	1.25	1.23	1.1	1.08	0.95	0.95	0.92	1	1.08	1.12	1.18	]	
Adjuste	ed infiltra	ation rat	e (allow	ing for sl	nelter ar	nd wind s	speed) :	= (21a) x	(22a)m					
	0.4	0.39	0.38	0.34	0.33	0.29	0.29	0.29	0.31	0.33	0.35	0.36		
	ate effec echanica		-	rate for t	he appl	cable ca	se							(23a)
				endix N. (2	3b) = (23;	a) x Fmv (e	equation	(N5)) , othe	rwise (23h	(23a) = (23a)			0	(23a)
								m Table 4h		(200)			0	(230)
			-	-	-			/HR) (24a		2b)m + (	23b) × [′	1 – (23c)	_	(200)
, (24a)m=	0	0	0	0	0	0	0	0	0	0	0	0		(24a)
b) If	balance	d mech	anical ve	entilation	without	heat red	covery (	(MV) (24k	)m = (2	2b)m + (	23b)		3	
(24b)m=	0	0	0	0	0	0	0	0	0	0	0	0	]	(24b)
,					•			ion from ( 4c) = (22		.5 × (23b	)	-	-	
(24c)m=	0	0	0	0	0	0	0	0	0	0	0	0	]	(24c)
								ion from 0.5 + [(2		0.5]			•	
(24d)m=	0.58	0.58	0.57	0.56	0.56	0.54	0.54	0.54	0.55	0.56	0.56	0.57	]	(24d)
Effec	ctive air	change	rate - ei	nter (24a	) or (24	o) or (24	c) or (2	4d) in bo	x (25)		•		-	
(25)m=	0.58	0.58	0.57	0.56	0.56	0.54	0.54	0.54	0.55	0.56	0.56	0.57	]	(25)
3. Hea	at losse	s and he	eat loss	paramet	er:									
ELEN	IENT	Gros area		Openin m		Net Ar A ,r		U-val W/m2		A X U (W/	K)	k-value kJ/m²⊷		A X k kJ/K
Doors						1.83	x	1.2	=	2.196				(26)
Window	ws Type	1				1.17	x	1/[1/( 1.4 )+	0.04] =	1.55				(27)
Window	ws Type	2				1.12	x	1/[1/( 1.4 )+	0.04] =	1.48				(27)
Window	ws Type	3				0.39	x	1/[1/( 1.4 )+	0.04] =	0.52				(27)
Window	ws Type	4				2.98	x	1/[1/( 1.4 )+	0.04] =	3.95				(27)
Window	ws Type	5				0.39	x	1/[1/( 1.4 )+	0.04] =	0.52				(27)
Window	ws Type	6				1.14	x	1/[1/( 1.4 )+	0.04] =	1.51				(27)
Window	ws Type	7				1.25	x	1/[1/( 1.4 )+	0.04] =	1.66				(27)
Floor						36.25	5 X	0.11	=	3.9875				(28)
Walls		84.0	02	10.2	7	73.75	5 X	0.19	=	14.01				(29)
Roof		36.2	25	0		36.25	5 X	0.11	=	3.99				(30)
Total a	rea of e	lements	s, m²			156.5	2							(31)
Party v	vall					39.42	<u>2</u> X	0	=	0				(32)
Interna	l floor					36.25	5							(32d)
				effective wi nternal wal			lated usin	ng formula 1	1/[(1/U-valu	ıe)+0.04] a	as given in	paragraph	h 3.2	
Fabric	heat los	s, W/K	= S (A x	U)				(26)(30	) + (32) =				35.3	37 (33)
Heat ca	apacity	Cm = S	(A x k )						((28).	(30) + (32	2) + (32a).	(32e) =	16817	.15 <mark>(34)</mark>
Therma	al mass	parame	eter (TMI	P = Cm -	- TFA) ii	ר kJ/m²K			Indica	tive Value	: Low		100	) (35)
For desig	gn assess	ments wh	nere the de	etails of the	construct	ion are no	t known p	precisely the	e indicative	e values of	TMP in Ta	able 1f		

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can be i	used inste	ad of a de	tailed calc	ulation.										
Therm	al bridg	es : S (L	x Y) cal	culated	using Ap	pendix l	<						13.85	(36)
if details	s of therma	al bridging	are not kr	own (36) =	= 0.05 x (3	1)								
Total f	abric he	at loss							(33) +	(36) =			49.22	(37)
Ventila	ation hea	at loss ca	alculated	monthl	/				(38)m	= 0.33 × (	25)m x (5)			
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
(38)m=	33.2	33.03	32.86	32.05	31.9	31.2	31.2	31.07	31.47	31.9	32.21	32.52		(38)
Heat t	ransfer o	coefficier	nt, W/K						(39)m	= (37) + (3	38)m			
(39)m=	82.42	82.25	82.08	81.28	81.13	80.43	80.43	80.3	80.7	81.13	81.43	81.75		
									,	Average =	Sum(39)1	12 /12=	81.27	(39)
Heat lo	oss para	meter (H	HLP), W	/m²K					(40)m	= (39)m ÷	- (4)			
(40)m=	1.14	1.13	1.13	1.12	1.12	1.11	1.11	1.11	1.11	1.12	1.12	1.13		_
Numb	er of day	/s in moi	nth (Tab	le 1a)					,	Average =	Sum(40)1.	12 /12=	1.12	(40)
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
(41)m=	31	28	31	30	31	30	31	31	30	31	30	31		(41)
		1	1	1			1			Į	Į	1	1	
1 \\/	otor hoo	ting enei	rav roqu	iromont:								kWh/ye	aar:	
- <del>1</del> . vvc	ater nea	ing ener	igy iequ	nement.								K V V I / Y V	-ai.	
		ipancy, l		•.		· · · · · · · · · · · · · · · · · · ·			- <i></i>			31		(42)
	A > 13. A £ 13.		+ 1.76 x	[1 - exp	(-0.0003	49 x (TF	-A -13.9	)2)] + 0.0	)013 x (	TFA -13.	.9)			
			ater usad	ae in litre	es per da	w Vd.av	erage =	(25 x N)	+ 36		88	.95		(43)
Reduce	the annua	al average	hot water	usage by	5% if the a	welling is	designed t	to achieve		se target o			l	
not mor	e that 125	litres per p	person pe	r day (all w	ater use, l	not and co	ld)							
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
Hot wat	er usage i	n litres per	r day for ea	ach month	Vd,m = fa	ctor from T	Table 1c x	(43)		-	-			
(44)m=	97.84	94.29	90.73	87.17	83.61	80.05	80.05	83.61	87.17	90.73	94.29	97.84		_
Francis	contont of	botwater	used as	a data d m	anthly 1	100 v Vd v		Tm / 2600			m(44) <sub>112</sub> =		1067.4	(44)
		1	1	1		-	1	0Tm / 3600		T			1	
(45)m=	145.1	126.91	130.96	114.17	109.55	94.53	87.6	100.52	101.72	118.55	129.4	140.52		<b>-</b>
lf instan	taneous v	vater heatii	na at noini	of use (no	hot water	storage)	enter () in	boxes (46)		Total = Su	m(45) <sub>112</sub> =	=	1399.53	(45)
			· ·	· ·						47.70	10.44	21.09	1	(46)
(46)m= Water	21.77 storage	19.04 loss:	19.64	17.13	16.43	14.18	13.14	15.08	15.26	17.78	19.41	21.08		(40)
	-		includir	ng any so	olar or W	/WHRS	storage	within sa	ame ves	sel		0		(47)
-		neating a					-					-	1	
		-			-			mbi boile	ers) ente	ər '0' in (	47)			
Water	storage	loss:												
a) If n	nanufact	urer's de	eclared I	oss facto	or is kno	wn (kWł	n/day):					0		(48)
Tempe	erature f	actor fro	m Table	2b								0		(49)
-		m water	-	-				(48) x (49)	=			0		(50)
,		urer's de		•									1	
		age loss			e 2 (KW	n/litre/da	ay)					0		(51)
	•	eating s from Ta		011 4.3								0	1	(52)
		actor fro		2b								0		(52)
•													1	

-	y lost fro r (50) or (		U U	e, kWh/ye	ear			(47) x (51)	) x (52) x (	53) =		0		(54) (55)
	r storage	. , .		for each	month			((56)m = (	55) × (41)ı	m		0		(00)
(56)m=		0	0	0	0	0	0	0	0	0	0	0		(56)
	der contains	-	-	-	-	-	-	-	-	-		-	ix H	(00)
(57)m=		0	0	0	0	0	0	0	0	0	0	0		(57)
					-	0	0	0	0	0				
	ry circuit	•	,			(FO)		NE (44)				0		(58)
	ry circuit						. ,	• • •		r thermo	stat)			
(59)m=	· · · ·										0	0		(59)
											-			, ,
	i loss ca			r	, 	r í			04.04	05 70	04.04	05.0		(61)
(61)m=		23.29	25.75	24.87	25.67	24.8	25.6	25.64	24.84	25.72	24.94	25.8		(61)
	· · · ·			<u> </u>		r		<u> </u>		, 	<u> </u>		(59)m + (61)m	(00)
(62)m=		150.2	156.7	139.04	135.22	119.33	113.2	126.17	126.56	144.26	154.34	166.33		(62)
	HW input o									r contribut	ion to wate	er heating)		
`	additiona	· · · · · ·		r	· · · · · ·	r	· · ·	i – – –	ŕ					(62)
(63)m=		0	0	0	0	0	0	0	0	0	0	0		(63)
•	ut from w	r		1		1								
(64)m=	170.92	150.2	156.7	139.04	135.22	119.33	113.2	126.17	126.56	144.26	154.34	166.33		<b>1</b> /2 ()
									out from wa				1702.27	(64)
Heat	gains fro	m water	heating	, kWh/m	onth 0.2	5 ´ [0.85	× (45)m	+ (61)m	n] + 0.8 ×	« [(46)m	+ (57)m	+ (59)m	]	
(65)m=	54.7	48.02	49.98	44.18	42.84	37.63	35.53	39.83	40.03	45.85	49.26	53.17		(65)
incl	ude (57)	m in calo	culation	of (65)m	only if c	ylinder i	s in the o	dwelling	or hot w	ater is fr	om com	munity h	eating	
5. Ir	nternal ga	ains (see	Table 5	5 and 5a	):									
Metal	o <mark>olic gain</mark>	is (Table	5), Wat	ts	_	-	-	-		-	-	-		
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
(66)m=	138.32	138.32	138.32	138.32	138.32	138.32	138.32	138.32	138.32	138.32	138.32	138.32		(66)
Lighti	ng gains	(calcula	ted in Ap	opendix	L, equat	ion L9 o	r L9a), a	lso see	Table 5					
(67)m=	50.57	44.92	36.53	27.66	20.67	17.45	18.86	24.51	32.9	41.78	48.76	51.98		(67)
Applia	ances ga	ins (calc	ulated ir	n Append	dix L, eq	uation L	13 or L1	3a), also	see Ta	ble 5	•			
(68)m=	303.07	306.22	298.29	281.42	260.13	240.11	226.74	223.59	231.52	248.39	269.69	289.7		(68)
Cook	ing gains	(calcula	ted in A	, ppendix	L, equat	tion L15	or L15a)	), also se	e Table	5				
(69)m=	<u> </u>	51.14	51.14	51.14	51.14	51.14	51.14	51.14	51.14	51.14	51.14	51.14		(69)
Pumr	s and fai	ns aains	(Table (	5a)										
(70)m=		3	3	3	3	3	3	3	3	3	3	3		(70)
Losse	es e.g. ev	u vaporatio	n (nega	ı tive valu	ı es) (Tab	ule 5)	1			1		1		
(71)m=		-92.21	-92.21	-92.21	-92.21	-92.21	-92.21	-92.21	-92.21	-92.21	-92.21	-92.21		(71)
					L	L					<u> </u>			1.1
	r heating	dains (T	able 5)											
(72)m=	r heating	<u> </u>	,	61.36	57.58	52.27	47.75	53.54	55.6	61.62	68.42	71.47		(72)
(72)m=	73.52	71.46	67.18	61.36	57.58	52.27	47.75 m + (67)m	53.54	55.6	61.62	68.42 1)m + (72)	71.47		(72)
	73.52	71.46	67.18	61.36 470.68	57.58				55.6 + (69)m + ( 420.26					(72)

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientati	ion:	Access Facto Table 6d	r	Area m²		Flux Table 6a		g_ Table 6b		FF Table 6c		Gains (W)	
East	0.9x	0.77	x	2.98	×	19.64	×	0.63	x	0.7	=	17.89	(76)
East	0.9x	0.77	x	1.14	x	19.64	x	0.63	x	0.7	=	6.84	(76)
East	0.9x	0.77	x	1.25	x	19.64	×	0.63	x	0.7	=	7.5	(76)
East	0.9x	0.77	x	2.98	x	38.42	×	0.63	x	0.7	=	34.99	(76)
East	0.9x	0.77	x	1.14	x	38.42	x	0.63	x	0.7	=	13.39	(76)
East	0.9x	0.77	x	1.25	x	38.42	×	0.63	x	0.7	=	14.68	(76)
East	0.9x	0.77	x	2.98	x	63.27	x	0.63	x	0.7	=	57.62	(76)
East	0.9x	0.77	x	1.14	×	63.27	×	0.63	x	0.7	=	22.04	(76)
East	0.9x	0.77	x	1.25	×	63.27	×	0.63	x	0.7	=	24.17	(76)
East	0.9x	0.77	x	2.98	x	92.28	×	0.63	x	0.7	=	84.04	(76)
East	0.9x	0.77	x	1.14	x	92.28	x	0.63	x	0.7	=	32.15	(76)
East	0.9x	0.77	x	1.25	x	92.28	×	0.63	x	0.7	=	35.25	(76)
East	0.9x	0.77	x	2.98	x	113.09	x	0.63	x	0.7	=	103	(76)
East	0.9x	0.77	x	1.14	x	113.09	×	0.63	x	0.7	=	39.4	(76)
East	0.9x	0.77	x	1.25	x	113.09	×	0.63	x	0.7	=	43.2	(76)
East	0.9x	0.77	x	2.98	x	115.77	x	0.63	x	0.7	=	105.44	(76)
East	0.9x	0.77	x	1.14	x	115.77	×	0.63	x	0.7	=	40.33	(76)
East	0.9x	0.77	x	1.25	x	115.77	x	0.63	x	0.7	=	44.23	(76)
East	0.9x	0.77	x	2.98	×	110.22	×	0.63	x	0.7	=	100.38	(76)
East	0.9x	0.77	x	1.14	x	110.22	×	0.63	x	0.7	=	38.4	(76)
East	0.9x	0.77	x	1.25	x	110.22	x	0.63	x	0.7	=	42.11	(76)
East	0.9x	0.77	x	2.98	x	94.68	×	0.63	x	0.7	=	86.22	(76)
East	0.9x	0.77	x	1.14	x	94.68	×	0.63	x	0.7	=	32.98	(76)
East	0.9x	0.77	x	1.25	x	94.68	×	0.63	x	0.7	=	36.17	(76)
East	0.9x	0.77	x	2.98	x	73.59	×	0.63	x	0.7	=	67.02	(76)
East	0.9x	0.77	x	1.14	×	73.59	×	0.63	x	0.7	=	25.64	(76)
East	0.9x	0.77	x	1.25	x	73.59	x	0.63	x	0.7	=	28.11	(76)
East	0.9x	0.77	x	2.98	x	45.59	×	0.63	X	0.7	=	41.52	(76)
East	0.9x	0.77	x	1.14	x	45.59	×	0.63	x	0.7	=	15.88	(76)
East	0.9x		x	1.25	x	45.59	×	0.63	x	0.7	=	17.42	(76)
East	0.9x		x	2.98	x	24.49	×	0.63	x	0.7	=	22.3	(76)
East	0.9x		x	1.14	x	24.49	×	0.63	x	0.7	=	8.53	(76)
East	0.9x		x	1.25	x	24.49	×	0.63	x	0.7	=	9.36	(76)
East	0.9x	-	x	2.98	x	16.15	×	0.63	x	0.7	=	14.71	(76)
East	0.9x		x	1.14	×	16.15	×	0.63	x	0.7	=	5.63	(76)
East	0.9x	-	x	1.25	x	16.15	×	0.63	x	0.7	=	6.17	(76)
South	0.9x		x	0.39	×	46.75	×	0.63	x	0.7	=	5.57	(78)
South	0.9x		x	0.39	x	46.75	×	0.63	x	0.7	=	5.57	(78)
South	0.9x	0.77	x	0.39	x	76.57	x	0.63	x	0.7	=	9.13	(78)

South         0.00         0.07         ×         0.63         ×         0.643         ×         0.07         =         0.13         (7)           South         0.37         0.77         ×         0.39         ×         0.763         ×         0.63         ×         0.77         =         0.1162         (7)           South         0.37         0.77         ×         0.39         ×         110.23         ×         0.633         ×         0.77         =         0.13.14         (7)           South         0.37         0.77         ×         0.39         ×         111.427         ×         0.633         ×         0.77         =         13.14         (7)           South         0.36         0.77         ×         0.39         ×         111.657         ×         0.633         ×         0.77         =         13.18         (7)           South         0.36         0.77         ×         0.39         ×         10.661         ×         0.633         ×         0.77         =         11.267         (7)           South         0.36         0.77         ×         0.39         ×         10.661         ×         <	Couth	Г		1		1						1		
Date         Date <th< td=""><td>South</td><td>0.9x</td><td>0.77</td><td>X</td><td>0.39</td><td>X</td><td>76.57</td><td>х</td><td>0.63</td><td>X</td><td>0.7</td><td>=</td><td>9.13</td><td>(78)</td></th<>	South	0.9x	0.77	X	0.39	X	76.57	х	0.63	X	0.7	=	9.13	(78)
South         Date         Date <thdate< th="">         Date         Date         <th< td=""><td></td><td></td><td>0.77</td><td>X</td><td>0.39</td><td>X</td><td>97.53</td><td>X</td><td>0.63</td><td>X</td><td>0.7</td><td>=</td><td>11.62</td><td>=</td></th<></thdate<>			0.77	X	0.39	X	97.53	X	0.63	X	0.7	=	11.62	=
South         0.82         0.77         ×         0.02         ×         0.03         ×         0.03         ×         0.03         0.77         ×         0.03         × <th0.03< th="">         ×</th0.03<>			0.77	×	0.39	X	97.53	X	0.63	X	0.7	=	11.62	4
South         O.X         O.77         ×         O.02         VILL         VILL         O.63         ×         O.77         =         O.13.69         (78)           South         0.8x         0.77         ×         0.39         ×         114.87         ×         0.63         ×         0.77         =         13.69         (78)           South         0.8x         0.77         ×         0.39         ×         110.55         ×         0.63         ×         0.77         =         13.18         (78)           South         0.8x         0.77         ×         0.39         ×         106.01         ×         0.63         ×         0.77         =         12.287         (78)           South         0.8x         0.77         ×         0.39         ×         106.81         ×         0.63         ×         0.77         =         12.287         (78)           South         0.8x         0.77         ×         0.39         ×         101.89         ×         0.63         ×         0.77         =         12.14         (78)           South         0.8x         0.77         ×         0.39         ×         55.42		0.9x	0.77	x	0.39	x	110.23	x	0.63	x	0.7	=	13.14	(78)
South         0.3         0.33         ×         11407         ×         0.033         ×         11407           South         0.3         0.77         ×         0.33         ×         110.55         ×         0.63         ×         0.77         =         13.18         (78)           South         0.3         0.77         ×         0.33         ×         110.55         ×         0.63         ×         0.77         =         13.18         (78)           South         0.3         0.77         ×         0.33         ×         110.55         ×         0.63         ×         0.77         =         12.57         (78)           South         0.3         0.77         ×         0.33         ×         104.89         ×         0.63         ×         0.77         =         12.57         (78)           South         0.3         0.77         ×         0.39         ×         104.89         ×         0.63         ×         0.77         =         12.41         (78)           South         0.3         0.77         ×         0.39         ×         82.59         ×         0.63         ×         0.77         9.84 </td <td></td> <td>0.9x</td> <td>0.77</td> <td>x</td> <td>0.39</td> <td>×</td> <td>110.23</td> <td>x</td> <td>0.63</td> <td>x</td> <td>0.7</td> <td>=</td> <td>13.14</td> <td>(78)</td>		0.9x	0.77	x	0.39	×	110.23	x	0.63	x	0.7	=	13.14	(78)
South         0.9x         0.77         ×         0.39         ×         110.55         ×         0.63         ×         0.77         =         13.18         (78)           South         0.9x         0.77         ×         0.39         ×         110.55         ×         0.63         ×         0.77         =         13.18         (78)           South         0.9x         0.77         ×         0.39         ×         106.01         ×         0.63         ×         0.77         =         12.87         (78)           South         0.9x         0.77         ×         0.39         ×         104.89         ×         0.63         ×         0.77         =         12.5         (78)           South         0.9x         0.77         ×         0.39         ×         101.89         ×         0.63         ×         0.77         =         12.14         (78)           South         0.9x         0.77         ×         0.39         ×         55.42         ×         0.63         ×         0.77         =         9.84         (78)           South         0.9x         0.77         ×         0.39         ×         55.		0.9x	0.77	x	0.39	x	114.87	x	0.63	x	0.7	=	13.69	(78)
South         O.S.         O.S. <t< td=""><td></td><td>0.9x</td><td>0.77</td><td>x</td><td>0.39</td><td>×</td><td>114.87</td><td>x</td><td>0.63</td><td>x</td><td>0.7</td><td>=</td><td>13.69</td><td>(78)</td></t<>		0.9x	0.77	x	0.39	×	114.87	x	0.63	x	0.7	=	13.69	(78)
South         0.000         x         0.000         x         0.000         x         0.01         x         0.02         x         0.02         x         0.02         x         0.02         0.77         x         0.03         x         0.01         x         0.02         0.77         x         0.03         x         0.02         0.77         x         0.03         x         0.02         0.77         x         0.03         x         0.07         x         0.03         x         0.77         x	South	0.9x	0.77	x	0.39	x	110.55	x	0.63	x	0.7	=	13.18	(78)
South         0.5         0.77         x         0.39         x         108.01         x         0.63         x         0.77         s         12.5         (78)           South         0.9x         0.77         x         0.39         x         104.89         x         0.63         x         0.77         =         12.5         (78)           South         0.9x         0.77         x         0.39         x         104.89         x         0.63         x         0.77         =         12.5         (78)           South         0.9x         0.77         x         0.39         x         101.89         x         0.63         x         0.77         =         12.14         (78)           South         0.9x         0.77         x         0.39         x         55.42         x         0.63         x         0.77         =         9.84         (78)           South         0.9x         0.77         x         0.39         x         55.42         x         0.63         x         0.77         =         6.61         (78)           South         0.9x         0.77         x         0.39         x         40.44 <td>South</td> <td>0.9x</td> <td>0.77</td> <td>x</td> <td>0.39</td> <td>x</td> <td>110.55</td> <td>x</td> <td>0.63</td> <td>x</td> <td>0.7</td> <td>=</td> <td>13.18</td> <td>(78)</td>	South	0.9x	0.77	x	0.39	x	110.55	x	0.63	x	0.7	=	13.18	(78)
South         0.0.1         x         0.0.33         x         100.489         x         0.0.3         x         0.0.33         x         100.489         x         0.0.3         x         0.0.7         x         0.39         x         0.0.3         x         0.0.3         x         0.0.3         x         0.0.7         x         0.39         x         0.55.42         x         0.63         x         0.7         =         0.641         (78)           South         0.9         0.77         x         0.39         x         55.42         x         0.63         x         0.7         =         6.61         (78)           South         0.9         0.77         x         0.39         x         40.4         x         0.63         x         0.7         4.82 </td <td>South</td> <td>0.9x</td> <td>0.77</td> <td>x</td> <td>0.39</td> <td>x</td> <td>108.01</td> <td>x</td> <td>0.63</td> <td>x</td> <td>0.7</td> <td>=</td> <td>12.87</td> <td>(78)</td>	South	0.9x	0.77	x	0.39	x	108.01	x	0.63	x	0.7	=	12.87	(78)
South         0.9         0.77         ×         0.39         ×         101.89         ×         0.063         ×         0.77         ×         0.39         ×         101.89         ×         0.63         ×         0.77         ×         0.39         ×         101.89         ×         0.63         ×         0.77         ×         0.39         ×         101.89         ×         0.63         ×         0.77         =         12.14         (78)           South         0.9         0.77         ×         0.39         ×         82.59         ×         0.63         ×         0.77         =         9.84         (78)           South         0.9         0.77         ×         0.39         ×         55.42         ×         0.63         ×         0.77         =         6.61         (78)           South         0.9         0.77         ×         0.39         ×         40.4         ×         0.63         ×         0.77         4.82         (78)           South         0.9         0.77         ×         0.39         ×         40.4         ×         0.63         ×         0.77         4.82         (78)           <	South	0.9x	0.77	x	0.39	x	108.01	x	0.63	x	0.7	=	12.87	(78)
South         0.9x         0.77         x         0.39         x         101.89         x         0.63         x         0.77         =         12.14         (78)           South         0.9x         0.77         x         0.39         x         101.89         x         0.63         x         0.77         =         12.14         (78)           South         0.9x         0.77         x         0.39         x         82.59         x         0.63         x         0.77         =         9.84         (78)           South         0.9x         0.77         x         0.39         x         55.42         x         0.63         x         0.77         =         6.61         (78)           South         0.9x         0.77         x         0.39         x         55.42         x         0.63         x         0.77         =         6.61         (78)           South         0.9x         0.77         x         0.39         x         40.4         x         0.63         x         0.77         =         4.82         (78)           West         0.9x         0.77         x         1.17         x         9.84	South	0.9x	0.77	x	0.39	x	104.89	x	0.63	x	0.7	=	12.5	(78)
South       0.9x       0.77       x       0.39       x       101.89       x       0.63       x       0.77       =       12.14       (78)         South       0.9x       0.77       x       0.39       x       82.59       x       0.63       x       0.77       =       9.84       (78)         South       0.9x       0.77       x       0.39       x       82.59       x       0.63       x       0.77       =       9.84       (78)         South       0.9x       0.77       x       0.39       x       55.42       x       0.63       x       0.77       =       6.61       (78)         South       0.9x       0.77       x       0.39       x       54.2       x       0.63       x       0.77       =       4.82       (78)         South       0.9x       0.77       x       0.39       x       40.4       x       0.63       x       0.77       =       4.82       (78)         South       0.9x       0.77       x       1.17       x       38.42       x       0.63       x       0.77       =       13.15       (80)       West       0.9x	South	0.9x	0.77	x	0.39	x	104.89	x	0.63	x	0.7	=	12.5	(78)
South         0.0         0.00 <th< td=""><td>South</td><td>0.9x</td><td>0.77</td><td>x</td><td>0.39</td><td>x</td><td>101.89</td><td>x</td><td>0.63</td><td>x</td><td>0.7</td><td>=</td><td>12.14</td><td>(78)</td></th<>	South	0.9x	0.77	x	0.39	x	101.89	x	0.63	x	0.7	=	12.14	(78)
South       0.x       0.77       x       0.39       x       0.63       x       0.77       =       9.84       76)         South       0.5x       0.77       x       0.39       x       55.42       x       0.63       x       0.77       =       6.61       (76)         South       0.5x       0.77       x       0.39       x       55.42       x       0.63       x       0.77       =       6.61       (76)         South       0.5x       0.77       x       0.39       x       40.4       x       0.63       x       0.77       =       6.61       (76)         South       0.5x       0.77       x       0.39       x       40.4       x       0.63       x       0.77       =       4.82       (76)         West       0.5x       0.77       x       1.17       x       19.64       x       0.63       x       0.77       =       13.74       (60)         West       0.5x       0.77       x       1.17       x       38.42       x       0.63       x       0.77       =       13.15       (60)         West       0.5x       0.77	South	0.9x	0.77	x	0.39	x	101.89	x	0.63	x	0.7	=	12.14	(78)
South       0.34       0.77       x       0.39       x       55.42       x       0.63       x       0.7       =       6.61       (78)         South       0.34       0.77       x       0.39       x       55.42       x       0.63       x       0.77       =       6.61       (78)         South       0.9x       0.77       x       0.39       x       40.4       x       0.63       x       0.7       =       6.61       (78)         South       0.9x       0.77       x       0.39       x       40.4       x       0.63       x       0.7       =       4.82       (78)         West       0.9x       0.77       x       1.17       x       19.64       x       0.63       x       0.7       =       6.72       (80)         West       0.9x       0.77       x       1.17       x       38.42       x       0.63       x       0.7       =       13.74       (80)         West       0.9x       0.77       x       1.17       x       38.42       x       0.63       x       0.7       =       13.15       (80)         West       0	South	0.9x	0.77	x	0.39	x	82.59	x	0.63	x	0.7	=	9.84	(78)
South0.17x0.33x55.42x0.63x0.7=6.61(78)South0.9x0.77x0.39x40.4x0.63x0.7=4.82(78)South0.9x0.77x0.39x40.4x0.63x0.7=4.82(78)West0.9x0.77x1.17x19.64x0.63x0.7=4.82(78)West0.9x0.77x1.12x19.64x0.63x0.7=6.72(80)West0.9x0.77x1.12x19.64x0.63x0.7=6.72(80)West0.9x0.77x1.12x18.64x0.63x0.7=13.74(80)West0.9x0.77x1.17x38.42x0.63x0.7=13.74(80)West0.9x0.77x1.17x38.42x0.63x0.7=13.15(60)West0.9x0.77x1.17x63.27x0.63x0.7=21.66(60)West0.9x0.77x1.17x92.28x0.63x0.7=33.60(60)West0.9x0.77x1.17x113.09x0.6	South	0.9x	0.77	x	0.39	x	82.59	x	0.63	x	0.7	=	9.84	(78)
South       0.9x       0.77       x       0.39       x       40.4       x       0.63       x       0.77       =       4.82       (78)         South       0.9x       0.77       x       0.39       x       40.4       x       0.63       x       0.77       =       4.82       (78)         West       0.9x       0.77       x       0.117       x       19.64       x       0.63       x       0.77       =       6.72       (80)         West       0.9x       0.77       x       1.12       x       19.64       x       0.63       x       0.77       =       6.72       (80)         West       0.9x       0.77       x       1.12       x       38.42       x       0.63       x       0.77       =       13.15       (60)         West       0.9x       0.77       x       1.12       x       63.27       x       0.63       x       0.77       =       21.66       (60)         West       0.9x       0.77       x       1.17       x       92.28       0.63       x       0.77       =       31.59       (60)         West       0.9x	South	0.9x	0.77	x	0.39	x	55.42	x	0.63	x	0.7	=	6.61	(78)
South $0.11$ $1$ $0.33$ $1$ $0.04$ $1$ $0.03$ $1$ $0.17$ $1.02$ $1$	South	0.9x	0.77	x	0.39	x	55.42	x	0.63	x	0.7	=	6.61	(78)
West $0.9x$ $0.77$ $x$ $1.17$ $x$ $19.64$ $x$ $0.63$ $x$ $0.7$ $=$ $7.02$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $19.64$ $x$ $0.63$ $x$ $0.7$ $=$ $6.72$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $19.64$ $x$ $0.63$ $x$ $0.7$ $=$ $6.72$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $38.42$ $x$ $0.63$ $x$ $0.7$ $=$ $13.74$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $38.42$ $x$ $0.63$ $x$ $0.7$ $=$ $13.74$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $38.42$ $x$ $0.63$ $x$ $0.7$ $=$ $13.15$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $63.27$ $x$ $0.63$ $x$ $0.7$ $=$ $22.62$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $63.27$ $x$ $0.63$ $x$ $0.7$ $=$ $21.66$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $31.59$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $40.44$ $(80)$ We	South	0.9x	0.77	x	0.39	x	40.4	x	0.63	x	0.7	=	4.82	(78)
West $0.9x$ $0.77$ $x$ $1.12$ $x$ $19.64$ $x$ $0.63$ $x$ $0.77$ $z$ $6.72$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $38.42$ $x$ $0.63$ $x$ $0.77$ $z$ $13.74$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $38.42$ $x$ $0.63$ $x$ $0.77$ $z$ $13.74$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $38.42$ $x$ $0.63$ $x$ $0.77$ $z$ $13.15$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $63.27$ $x$ $0.63$ $x$ $0.77$ $z$ $22.62$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $63.27$ $x$ $0.63$ $x$ $0.77$ $z$ $21.66$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $92.28$ $x$ $0.63$ $x$ $0.77$ $z$ $33.60$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $113.09$ $x$ $0.63$ $x$ $0.77$ $z$ $40.44$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $113.09$ $x$ $0.63$ $x$ $0.77$ $z$ $41.4$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $115.77$ $x$ $0.63$ $x$ $0.7$ $z$ $38.71$ $(80)$ West	South	0.9x	0.77	x	0.39	x	40.4	x	0.63	x	0.7	=	4.82	(78)
West $0.9x$ $0.77$ $x$ $1.12$ $x$ $1.00x$ $x$ $0.00x$ $x$ $0.11$ $0.12$ $(0.12)$	West	0.9x	0.77	x	1.17	x	19.64	x	0.63	x	0.7	=	7.02	(80)
West $0.9x$ $0.77$ x $1.12$ x $38.42$ x $0.63$ x $0.77$ $=$ $13.15$ $(80)$ West $0.9x$ $0.77$ x $1.12$ x $38.42$ x $0.63$ x $0.7$ $=$ $22.62$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $63.27$ x $0.63$ x $0.7$ $=$ $22.62$ $(80)$ West $0.9x$ $0.77$ x $1.12$ x $63.27$ x $0.63$ x $0.7$ $=$ $22.62$ $(80)$ West $0.9x$ $0.77$ x $1.12$ x $63.27$ x $0.63$ x $0.7$ $=$ $21.66$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $92.28$ x $0.63$ x $0.7$ $=$ $31.59$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $113.09$ x $0.63$ x $0.7$ $=$ $40.44$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $115.77$ $x$ $0.63$ x $0.7$ $=$ $39.63$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $115.77$ $x$ $0.63$ x $0.7$ $=$ $39.63$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $110.22$ x $0.63$ x $0.7$ $=$ $39.63$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x<	West	0.9x	0.77	x	1.12	x	19.64	x	0.63	x	0.7	=	6.72	(80)
West       0.9x       0.77       x       1.17       x       63.27       x       0.63       x       0.7       =       22.62       (80)         West       0.9x       0.77       x       1.12       x       63.27       x       0.63       x       0.7       =       22.62       (80)         West       0.9x       0.77       x       1.12       x       63.27       x       0.63       x       0.7       =       22.62       (80)         West       0.9x       0.77       x       1.17       x       92.28       x       0.63       x       0.7       =       33       (80)         West       0.9x       0.77       x       1.17       x       92.28       x       0.63       x       0.7       =       31.59       (80)         West       0.9x       0.77       x       1.17       x       113.09       x       0.63       x       0.7       =       41.4       (80)         West       0.9x       0.77       x       1.17       x       115.77       x       0.63       x       0.7       =       39.63       (80)         West       0.	West	0.9x	0.77	x	1.17	x	38.42	x	0.63	x	0.7	=	13.74	(80)
West $0.9x$ $0.77$ $x$ $1.12$ $x$ $63.27$ $x$ $0.63$ $x$ $0.7$ $z$ $21.66$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $33$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $33$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $31.59$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $113.09$ $x$ $0.63$ $x$ $0.7$ $=$ $40.44$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $113.09$ $x$ $0.63$ $x$ $0.7$ $=$ $41.4$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $115.77$ $x$ $0.63$ $x$ $0.7$ $=$ $41.4$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $110.22$ $x$ $0.63$ $x$ $0.7$ $=$ $37.73$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $94.68$ $x$ $0.63$ $x$ $0.7$ $=$ $33.85$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $73.59$ $x$ $0.63$ $x$ $0.7$ $=$ $32.41$ $(80)$ Wes	West	0.9x	0.77	x	1.12	x	38.42	x	0.63	x	0.7	=	13.15	(80)
West $0.9x$ $0.77$ $x$ $1.17$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $33$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $31.59$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $31.59$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $113.09$ $x$ $0.63$ $x$ $0.7$ $=$ $40.44$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $113.09$ $x$ $0.63$ $x$ $0.7$ $=$ $38.71$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $115.77$ $x$ $0.63$ $x$ $0.7$ $=$ $41.4$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $115.77$ $x$ $0.63$ $x$ $0.7$ $=$ $39.63$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $110.22$ $x$ $0.63$ $x$ $0.7$ $=$ $33.85$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $94.68$ $x$ $0.63$ $x$ $0.7$ $=$ $32.41$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $73.59$ $x$ $0.63$ $x$ $0.7$ $=$ $26.31$ $(80)$ <t< td=""><td>West</td><td>0.9x</td><td>0.77</td><td>x</td><td>1.17</td><td>x</td><td>63.27</td><td>x</td><td>0.63</td><td>x</td><td>0.7</td><td>=</td><td>22.62</td><td>(80)</td></t<>	West	0.9x	0.77	x	1.17	x	63.27	x	0.63	x	0.7	=	22.62	(80)
West $0.9x$ $0.77$ $x$ $1.12$ $x$ $92.28$ $x$ $0.63$ $x$ $0.7$ $=$ $31.59$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $113.09$ $x$ $0.63$ $x$ $0.7$ $=$ $40.44$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $113.09$ $x$ $0.63$ $x$ $0.7$ $=$ $40.44$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $113.09$ $x$ $0.63$ $x$ $0.7$ $=$ $40.44$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $115.77$ $x$ $0.63$ $x$ $0.7$ $=$ $41.4$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $115.77$ $x$ $0.63$ $x$ $0.7$ $=$ $39.63$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $110.22$ $x$ $0.63$ $x$ $0.7$ $=$ $39.41$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $94.68$ $x$ $0.63$ $x$ $0.7$ $=$ $32.41$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $73.59$ $x$ $0.63$ $x$ $0.7$ $=$ $32.41$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $73.59$ $x$ $0.63$ $x$ $0.7$ $=$ $26.31$ $(80)$ <t< td=""><td>West</td><td>0.9x</td><td>0.77</td><td>x</td><td>1.12</td><td>x</td><td>63.27</td><td>x</td><td>0.63</td><td>x</td><td>0.7</td><td>=</td><td>21.66</td><td>(80)</td></t<>	West	0.9x	0.77	x	1.12	x	63.27	x	0.63	x	0.7	=	21.66	(80)
West $0.9x$ $0.77$ x $1.17$ x $113.09$ x $0.63$ x $0.7$ = $40.44$ (80)West $0.9x$ $0.77$ x $1.12$ x $113.09$ x $0.63$ x $0.7$ = $38.71$ (80)West $0.9x$ $0.77$ x $1.17$ x $115.77$ x $0.63$ x $0.7$ = $41.4$ (80)West $0.9x$ $0.77$ x $1.17$ x $115.77$ x $0.63$ x $0.7$ = $39.63$ (80)West $0.9x$ $0.77$ x $1.12$ x $115.77$ x $0.63$ x $0.7$ = $39.63$ (80)West $0.9x$ $0.77$ x $1.12$ x $110.22$ x $0.63$ x $0.7$ = $39.41$ (80)West $0.9x$ $0.77$ x $1.12$ x $110.22$ x $0.63$ x $0.7$ = $37.73$ (80)West $0.9x$ $0.77$ x $1.17$ x $94.68$ x $0.63$ x $0.7$ = $32.41$ (80)West $0.9x$ $0.77$ x $1.17$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ (80)West $0.9x$ $0.77$ x $1.17$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ (80)West $0.9x$ $0.77$ x $1.17$ x $45.59$ x $0.63$ <td>West</td> <td>0.9x</td> <td>0.77</td> <td>x</td> <td>1.17</td> <td>x</td> <td>92.28</td> <td>x</td> <td>0.63</td> <td>x</td> <td>0.7</td> <td>=</td> <td>33</td> <td>(80)</td>	West	0.9x	0.77	x	1.17	x	92.28	x	0.63	x	0.7	=	33	(80)
West $0.9x$ $0.77$ x $1.12$ x $113.09$ x $0.63$ x $0.7$ = $38.71$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $115.77$ x $0.63$ x $0.7$ = $41.4$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $115.77$ x $0.63$ x $0.7$ = $39.63$ $(80)$ West $0.9x$ $0.77$ x $1.12$ x $115.77$ x $0.63$ x $0.7$ = $39.63$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $110.22$ x $0.63$ x $0.7$ = $39.41$ $(80)$ West $0.9x$ $0.77$ x $1.12$ x $110.22$ x $0.63$ x $0.7$ = $37.73$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $94.68$ x $0.63$ x $0.7$ = $32.41$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ $(80)$ West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $25.19$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $45.59$ x $0.63$ x $0.7$ = $16.3$ $(80)$	West	0.9x	0.77	x	1.12	x	92.28	x	0.63	x	0.7	=	31.59	(80)
West       0.9x       0.77       x       1.17       x       115.77       x       0.63       x       0.7       =       41.4       (80)         West       0.9x       0.77       x       1.12       x       115.77       x       0.63       x       0.77       =       41.4       (80)         West       0.9x       0.77       x       1.12       x       115.77       x       0.63       x       0.7       =       41.4       (80)         West       0.9x       0.77       x       1.12       x       110.22       x       0.63       x       0.7       =       39.63       (80)         West       0.9x       0.77       x       1.12       x       110.22       x       0.63       x       0.7       =       39.41       (80)         West       0.9x       0.77       x       1.12       x       110.22       x       0.63       x       0.7       =       33.85       (80)         West       0.9x       0.77       x       1.17       x       94.68       x       0.63       x       0.7       =       32.41       (80)         West	West	0.9x	0.77	x	1.17	x	113.09	x	0.63	x	0.7	=	40.44	(80)
West $0.9x$ $0.77$ $x$ $1.12$ $x$ $115.77$ $x$ $0.63$ $x$ $0.7$ $=$ $39.63$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $110.22$ $x$ $0.63$ $x$ $0.7$ $=$ $39.41$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $110.22$ $x$ $0.63$ $x$ $0.7$ $=$ $39.41$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $110.22$ $x$ $0.63$ $x$ $0.7$ $=$ $37.73$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $94.68$ $x$ $0.63$ $x$ $0.7$ $=$ $33.85$ $(80)$ West $0.9x$ $0.77$ $x$ $1.12$ $x$ $94.68$ $x$ $0.63$ $x$ $0.7$ $=$ $32.41$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $73.59$ $x$ $0.63$ $x$ $0.7$ $=$ $26.31$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $73.59$ $x$ $0.63$ $x$ $0.7$ $=$ $25.19$ $(80)$ West $0.9x$ $0.77$ $x$ $1.17$ $x$ $45.59$ $x$ $0.63$ $x$ $0.7$ $=$ $16.3$ $(80)$	West	0.9x	0.77	x	1.12	x	113.09	x	0.63	x	0.7	=	38.71	(80)
West       0.9x       0.77       x       1.17       x       110.22       x       0.63       x       0.77       =       39.41       (80)         West       0.9x       0.77       x       1.12       x       110.22       x       0.63       x       0.77       =       39.41       (80)         West       0.9x       0.77       x       1.12       x       110.22       x       0.63       x       0.77       =       37.73       (80)         West       0.9x       0.77       x       1.17       x       94.68       x       0.63       x       0.77       =       33.85       (80)         West       0.9x       0.77       x       1.12       x       94.68       x       0.63       x       0.77       =       32.41       (80)         West       0.9x       0.77       x       1.17       x       73.59       x       0.63       x       0.77       =       26.31       (80)         West       0.9x       0.77       x       1.12       x       73.59       x       0.63       x       0.77       =       25.19       (80)         West	West	0.9x	0.77	x	1.17	x	115.77	x	0.63	x	0.7	=	41.4	(80)
West $0.9x$ $0.77$ x $1.12$ x $110.22$ x $0.63$ x $0.7$ = $37.73$ (80)West $0.9x$ $0.77$ x $1.17$ x $94.68$ x $0.63$ x $0.7$ = $33.85$ (80)West $0.9x$ $0.77$ x $1.12$ x $94.68$ x $0.63$ x $0.7$ = $32.41$ (80)West $0.9x$ $0.77$ x $1.12$ x $94.68$ x $0.63$ x $0.7$ = $32.41$ (80)West $0.9x$ $0.77$ x $1.17$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ (80)West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $25.19$ (80)West $0.9x$ $0.77$ x $1.17$ x $45.59$ x $0.63$ x $0.7$ = $16.3$ (80)	West	0.9x	0.77	x	1.12	x	115.77	x	0.63	x	0.7	=	39.63	(80)
West $0.9x$ $0.77$ x $1.17$ x $94.68$ x $0.63$ x $0.7$ = $33.85$ (80)West $0.9x$ $0.77$ x $1.12$ x $94.68$ x $0.63$ x $0.7$ = $32.41$ (80)West $0.9x$ $0.77$ x $1.17$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ (80)West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ (80)West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $25.19$ (80)West $0.9x$ $0.77$ x $1.17$ x $45.59$ x $0.63$ x $0.7$ = $16.3$ (80)	West	0.9x	0.77	x	1.17	x	110.22	x	0.63	x	0.7	=	39.41	(80)
West $0.9x$ $0.77$ x $1.12$ x $94.68$ x $0.63$ x $0.7$ = $32.41$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ $(80)$ West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ $(80)$ West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $25.19$ $(80)$ West $0.9x$ $0.77$ x $1.17$ x $45.59$ x $0.63$ x $0.7$ = $16.3$ $(80)$	West	0.9x	0.77	x	1.12	x	110.22	x	0.63	x	0.7	=	37.73	(80)
West $0.9x$ $0.77$ x $1.17$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ (80)         West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $26.31$ (80)         West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $25.19$ (80)         West $0.9x$ $0.77$ x $1.17$ x $45.59$ x $0.63$ x $0.7$ = $16.3$ (80)	West	0.9x	0.77	x	1.17	×	94.68	x	0.63	×	0.7	=	33.85	(80)
West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $25.19$ (80)         West $0.9x$ $0.77$ x $1.12$ x $73.59$ x $0.63$ x $0.7$ = $25.19$ (80)         West $0.9x$ $0.77$ x $1.17$ x $45.59$ x $0.63$ x $0.7$ = $16.3$ (80)	West	0.9x	0.77	x	1.12	x	94.68	x	0.63	x	0.7	=	32.41	(80)
West $0.9x$ $0.77$ x $1.17$ x $45.59$ x $0.63$ x $0.7$ = $16.3$ (80)	West	0.9x	0.77	x	1.17	×	73.59	x	0.63	x	0.7	=	26.31	(80)
	West	0.9x	0.77	x	1.12	×	73.59	x	0.63	×	0.7	=	25.19	(80)
West       0.9x       0.77       x       1.12       x       45.59       x       0.63       x       0.7       =       15.6       (80)	West	0.9x	0.77	×	1.17	×	45.59	x	0.63	x	0.7	=	16.3	(80)
	West	0.9x	0.77	x	1.12	x	45.59	x	0.63	x	0.7	=	15.6	(80)

	F								. —		-, -				_
West	0.9x	0.77	;	· 1.	17	x	2	.4.49	×	0.63		0.7	=	8.76	(80)
West	0.9x	0.77	;	· 1.	12	x	2	24.49	×	0.63		0.7	=	8.38	(80)
West	0.9x	0.77		· 1.′	17	x	1	6.15	×	0.63	_ × _	0.7	=	5.78	(80)
West	0.9x	0.77	2	<b>1</b> .	12	x	1	6.15	x	0.63	x	0.7	=	5.53	(80)
	pains in 57.12	watts, ca 108.19		d for eac		1	07.07	1	. ,	Sum(74)m .	r Ó	70.54	47.44	l	(83)
(83)m=	-		171.37	242.3 ar (84)m =	292.13		97.37 83)m	283.77	246.64	196.56	126.41	70.54	47.44		(03)
(84)m=	584.53	631.03	673.62	<u>, ,</u>	730.76	Ť	07.44	, walls	648.53	616.82	578.44	557.64	560.83		(84)
							07.44	077.50	040.00	010.02	370.44	337.04	300.03		(01)
				e (heating											
		-	-	periods ii		-			ole 9, T	n1 (°C)				21	(85)
Utilisa				living are	1	ТÌ Т		,				<u> </u>			
	Jan	Feb	Mar	Apr	May	+	Jun	Jul	Aug	Sep	Oct	Nov	Dec		(22)
(86)m=	0.94	0.92	0.89	0.83	0.74		0.6	0.47	0.51	0.69	0.85	0.92	0.94		(86)
Mean	interna	l temper	ature ir	living ar	ea T1 (f	ollo	w ste	ps 3 to 7	in Tab	le 9c)				L	
(87)m=	18.95	19.16	19.53	20.03	20.46	2	20.78	20.92	20.9	20.67	20.12	19.45	18.9		(87)
Temp	erature	during h	eating	periods ii	n rest of	dw	elling	from Ta	ble 9, T	「h2 (°C)					
(88)m=	19.97	19.97	19.97	19.98	19.99	1	9.99	19.99	19.99	19.99	19.99	19.98	19.98		(88)
Utilis	ation fac	tor for a	ains for	rest of d	wellina.	h2.	.m (se	e Table	9a)	-		-	-		
(89)m=	0.93	0.91	0.87	0.8	0.7	<b>T</b>	0.54	0.38	0.42	0.63	0.82	0.9	0.93		(89)
Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)															
(90)m=	17.25	17.56	18.09	18.79	19.39	<b>T</b>	9.79	19.94	19.92	19.67	18.93	17.99	17.19		(90)
					ļ					1	L fLA = Livir	l ig area ÷ (•	4) =	0.17	(91)
Maar	interne		oturo (4	o # 4k ok	مام مارزم		~) fl	Δ <b>Τ</b> 4	. / 4 . 4						
(92)m=	17.55	17.83	18.34	or the wh	19.57	-	g) = 11 9.97	20.11	+ (1 - 1 20.09	19.84	19.14	18.25	17.49		(92)
										ere appro		10.25	17.49		(02)
(93)m=	17.4	17.68	18.19	18.86	19.42	1	9.82	19.96	19.94	19.69	18.99	18.1	17.34		(93)
	ace hea	ting requ	uiremer		<u> </u>	1					-	<u> </u>	I		
					re obtaiı	ned	l at ste	ep 11 of	Table 9	b, so tha	t Ti,m=(	76)m an	d re-cald	ulate	
the ut	tilisation	factor fo	or gains	using Ta	able 9a	_						,			
	Jan	Feb	Mar	Apr	May		Jun	Jul	Aug	Sep	Oct	Nov	Dec		
	r	tor for g	1	1		-					1			I	
(94)m=	0.9	0.88	0.84	0.77	0.67	(	0.52	0.38	0.41	0.61	0.78	0.87	0.91		(94)
	<u> </u>	· · · · ·	· · ·	94)m x (8	r'		~~~~							l	(05)
(95)m=	524.65	553.03	564.53		488.52		69.87	255.69	265.94	373.95	452.6	484.7	507.73		(95)
	<u> </u>	<u> </u>		nperature	ì	-		40.0	40.4		10.0	74	40	l	(06)
(96)m=	4.3	4.9	6.5	8.9	11.7		14.6	16.6	16.4	14.1	10.6	7.1	4.2		(96)
Heat (97)m=	· · · · · · · · · · · · · · · · · · ·	1051.53	an inter 959.9	809.17	erature, 626.64	-	n,VV = 19.47	=[(39)m : 270.14	x [(93)n 284.51	n— (96)m 451.18	680.49	895.55	1074.13		(97)
										7)m – (95			10/4.13		
(98)m=	412.91	334.99	294.16		102.76		0	11 = 0.02	4 X [(9)	0	169.55	295.82	421.41		
(00)11-		00 1.00		1	1		~	Ĺ	Ĭ	Ĭ	1		L		
									Tot	al per vear	(kWh/vea	r) = Sum(q)	8)1 50 40 =	2218 73	(98)
0	• • • • • • •			n kWh/m <sup>2</sup>	26.00-				Tot	al per year	(kWh/yea	r) = Sum(9	<b>98)</b> <sub>15,912</sub> =	2218.73 30.6	(98)

9a. Energ	gy req	uiremer	nts – Ind	ividual h	eating s	ystems i	ncluding	micro-C	CHP)					
Space I		•			, .									
				econdar		mentary	-	(000) 4	(204)				0	(201)
				nain syst	. ,			(202) = 1 -		(000)]			1	(202)
			-	main sys				(204) = (20	02) × [1 –	(203)] =			1	(204)
		-		ing syste									92.4	(206)
Efficien	cy of s	econda	ry/suppl	ementar	y heating	g system	ז, %			r			0	(208)
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/yea	ar
· –	12.91	334.99	ement (0 294.16	alculate	d above 102.76	0	0	0	0	169.55	295.82	421.41		
						0	0	0	0	109.00	290.02	421.41		(011)
(211)m =	46.87	362.54	4)] } X 318.35	202.53	111.21	0	0	0	0	183.5	320.15	456.07		(211)
											211) <sub>15,1012</sub>		2401.23	(211)
Space h	neating	g fuel (s	econdar	y), kWh/	month							l		]
= {[(98 <u>)</u> m	-			• /	-					-	-			
(215)m=	0	0	0	0	0	0	0	0	0	0	0	0		-
								Tota	l (kWh/yea	ar) =Sum(2	2 <b>15)</b> <sub>15,1012</sub>	2=	0	(215)
Water he			tor (oolo	what a d	hava)									
Output fr	70.92	150.2	156.7	139.04	135.22	119.33	113.2	126.17	126.56	144.26	154.34	166.33		
Efficiency	y of wa	ater hea	iter										87	(216)
(217)m=	89.1	89.05	88.93	88.7	88.27	87	87	87	87	88.6	88.95	89.13		(217)
Fuel for v		-												
(219)m = (219)m= 1		<u>m x 100</u> 168.67	) ÷ (217) 176.2	)m 156.76	153.18	137.16	130.12	145.02	145.47	162.83	173.52	186.61		
(210)11-1	01.00	100.07	17 0.2	100.70	100.10	107.10	100.12		I = Sum(2'		170.02	100.01	1927.38	(219)
Annual t	otals										Wh/year	r I	kWh/year	]()
Space he	eating	fuel use	ed, main	system	1								2401.23	]
Water he	ating	fuel use	d										1927.38	Ī
Electricity	y for p	umps, fa	ans and	electric	keep-ho	t						ľ		-
central l	heatin	g pump	:		-							30		(230c)
boiler w												45		(230e)
Total ele					r			sum	of (230a).	(230g) =			75	(231)
Electricity	y for lig	ghting		Ē									357.25	] (232)
Electricity	y gene	erated b	y PVs										-1364.85	(233)
Total deli	ivered	energy	for all u	ses (211	)(221)	+ (231)	+ (232).	(237b)	=				3396	(338)
10a. Fu	el cos	ts - ind <u>i</u> v	/idual he	eating sy	stems:									_
						Fu	el			Fuel P	rice		Fuel Cost	

	<b>Fuel</b> kWh/year	Fuel Price (Table 12)	<b>Fuel Cost</b> £/year
Space heating - main system 1	(211) x	3.48 × 0.01 =	83.56 (240)
Space heating - main system 2	(213) x	0 x 0.01 =	0 (241)

Space heating - secondary	(21	5)	x		13.19	x 0.01 =	0	(242)
Water heating cost (other fuel)	(21	9)			3.48	x 0.01 =	67.07	(247)
Pumps, fans and electric keep-hot	(23	1)			13.19	x 0.01 =	9.89	(249)
(if off-peak tariff, list each of (230a) to (23	30g) separatel		s applicable and	apply		ording to $\frac{1}{x 0.01} =$		(050)
Energy for lighting Additional standing charges (Table 12)	(20)	~)			13.19	x 0.01 =	47.12	(250)
Additional standing charges (Table 12)							120	(251)
			(233) to (235) x)		13.19	x 0.01 =	-180.02	(252)
Appendix Q items: repeat lines (253) and <b>Total energy cost</b>	1 (254) as need (245)(247) + (25						147.63	(255)
11a. SAP rating - individual heating sys							147.00	(===)
Energy cost deflator (Table 12)							0.42	(256)
	[(255) x (256)] ÷ [(	(4) -	+ 45.0] =				0.42	(257)
SAP rating (Section 12)							92.64	(258)
12a. CO2 emissions – Individual heating	g systems incl	udi	ng micro-CHP					
	En kW		<b>gy</b> 'year		Emission fa		<b>Emissic</b> kg CO2/	-
Space heating (main system 1)	(21	1)	x		0.216	=	518.66	(261)
Space heating (secondary)	(21	5)	x		0.519	=	0	(263)
Water heating	(21	9)	x		0.216	=	416.31	(264)
Space and water heating	(26	1) +	· (262) + (263) + (264	4) =			934.98	(265)
Electricity for pumps, fans and electric ke	ep-hot (23	1)	x		0.519	=	38.93	(267)
Electricity for lighting	(23)	2)	x		0.519	=	185.41	(268)
Energy saving/generation technologies Item 1					0.519	=	-708.36	(269)
Total CO2, kg/year				sum of	(265)(271) =		450.96	(272)
CO2 emissions per m <sup>2</sup>				(272) ÷	- (4) =		6.22	(273)
El rating (section 14)							95	(274)
13a. Primary Energy								
	En kV		<b>gy</b> 'year		Primary factor		<b>P. Ener</b> g kWh/yea	
Space heating (main system 1)	(21	1)	x		1.22	=	2929.49	(261)
Space heating (secondary)	(21	5)	x		3.07	=	0	(263)
Energy for water heating	(21	9)	x		1.22	=	2351.4	(264)
Space and water heating			(262) + (263) + (264	4) =			5280.9	(265)
Electricity for pumps, fans and electric ke	ep-hot (23	1)	x		3.07	=	230.25	(267)
Electricity for lighting	(23)	2)	x		0	=	1096.75	(268)

 Energy saving/generation technologies

 Item 1
 3.07 =
 -4190.08 (269)

 'Total Primary Energy
 sum of (265)...(271) =
 2417.81 (272)

 Primary energy kWh/m²/year
 (272) ÷ (4) =
 33.35 (273)

## **SAP 2012 Overheating Assessment**

Calculated by Stroma FSAP 2012 program, produced and printed on 29 November 2022

#### Property Details: Plot 33

Dwelling type:	Semi-detached House	
Located in:	England	
Region:	East Anglia	
Cross ventilation possible:	Yes	
Number of storeys:	2	
Front of dwelling faces:	West	
Overshading:	Average or unknown	
Overhangs:	None	
Thermal mass parameter:	Indicative Value Low	
Night ventilation:	False	
Blinds, curtains, shutters:	Dark-coloured curtain or roller blind	
Ventilation rate during hot weather (ach):	3 (Windows open half the time)	
Overheating Details:		
Summer ventilation heat loss coefficient:	172.26	(P1)

49.2 221.48

Summer ventilation heat loss coefficient:	
Transmission heat loss coefficient:	
Summer heat loss coefficient:	

#### Overhangs:

Orientation:	Ratio:	Z_overhangs:
West (W_1)	0	1
West (W_2)	0	1
South (W_3)	0	1
East (W_4)	0	1
South (W_5)	0	1
East (W_6)	0	1
East (W_7)	0	1

#### Solar shading:

Orientation:	Z blind	ls:	Solar access:	Ove	erhangs:	Z summer:	
West (W_1)	0.85		0.9	1		0.76	(P8)
West (W_2)	0.85		0.9	1		0.76	(P8)
South (W_3)	0.85		0.9	1		0.76	(P8)
East (W_4)	0.85		0.9	1		0.76	(P8)
South (W_5)	0.85		0.9	1		0.76	(P8)
East (W_6)	0.85		0.9	1		0.76	(P8)
East (W_7)	0.85		0.9	1		0.76	(P8)
Solar gains:							
Orientation		Area	Flux	<b>g_</b>	FF	Shading	Gains
West (W_1)	0.9 x	1.17	119.47	0.63	0.7	0.76	42.44
West (W_2)	0.9 x	1.12	119.47	0.63	0.7	0.76	40.63
South (W_3)	0.9 x	0.39	114.84	0.63	0.7	0.76	13.6
East (W_4)	0.9 x	2.98	119.47	0.63	0.7	0.76	108.1
South (W_5)	0.9 x	0.39	114.84	0.63	0.7	0.76	13.6
East (W_6)	0.9 x	1.14	119.47	0.63	0.7	0.76	41.35
East (W_7)	0.9 x	1.25	119.47	0.63	0.7	0.76	45.34
$\cdot = \cdot$						Total	305.06 <b>(P3/P4)</b>
Internal gains:							
				J	une	July	August
Internal gains					07.07	390.59	398.89
Total summer gains					29.87	695.65	666.4 <b>(P5)</b>

(P2)

## SAP 2012 Overheating Assessment

Summer gain/loss ratio	3.3	3.14	3.01	(P6)
Mean summer external temperature (East Anglia)	15.4	17.6	17.6	
Thermal mass temperature increment	1.3	1.3	1.3	
Threshold temperature	20	22.04	21.91	(P7)
Likelihood of high internal temperature	Not significant	Medium	Slight	

Assessment of likelihood of high internal temperature:

Medium