### **Regulations Compliance Report**



Approved Document L1A, 2013 Edition, England assessed by Stroma FSAP 2012 program, Version: 1.0.4.23 Printed on 26 February 2020 at 15:56:08

Project Information:

Assessed By: Matthew Stainrod (STRO023501) **Building Type:** Flat

Dwelling Details:

**NEW DWELLING DESIGN STAGE** 

Total Floor Area: 73.43m<sup>2</sup>

Site Reference: Tye Green Plot Reference: 08-19-79354 Plot 149 - Type A

Plot 149 - Type A, Tye Green Address:

Client Details:

Name: Countryside Properties

Address: Countryside House, The Drive, Brentwood, CM13 3AT

This report covers items included within the SAP calculations.

It is not a complete report of regulations compliance.

1a TER and DER

Fuel for main heating system: Mains gas

Fuel factor: 1.00 (mains gas)

18.97 kg/m<sup>2</sup> Target Carbon Dioxide Emission Rate (TER)

Dwelling Carbon Dioxide Emission Rate (DER) 16.94 kg/m<sup>2</sup> OK

1b TFEE and DFEE

Target Fabric Energy Efficiency (TFEE) 51.0 kWh/m<sup>2</sup>

Dwelling Fabric Energy Efficiency (DFEE) 43.1 kWh/m<sup>2</sup>

OK

2 Fabric U-values

Element	Average	Highest	
External wall	0.22 (max. 0.30)	0.24 (max. 0.70)	OK
Floor	0.15 (max. 0.25)	0.15 (max. 0.70)	OK
Roof	(no roof)		
Openings	1.16 (max. 2.00)	1.20 (max. 3.30)	OK

2a Thermal bridging

Thermal bridging calculated from linear thermal transmittances for each junction

3 Air permeability

Air permeability at 50 pascals 5.00 (design value)

OK Maximum 10.0

4 Heating efficiency

Main Heating system: Database: (rev 455, product index 018203):

Boiler systems with radiators or underfloor heating - mains gas

Brand name: Potterton

Model: Assure

Model qualifier: 25 Combi

(Combi)

Efficiency 89.0 % SEDBUK2009

Minimum 88.0 % OK

Secondary heating system: None

# **Regulations Compliance Report**



5 Cylinder insulation			
Hot water Storage:	No cylinder		
6 Controls			
Space heating controls	TTZC by plumbing and	electrical services	ОК
Hot water controls:	No cylinder thermostat		
	No cylinder		
Boiler interlock:	Yes		OK
7 Low energy lights			
Percentage of fixed lights	with low-energy fittings	100.0%	
Minimum		75.0%	OK
8 Mechanical ventilation			
Continuous extract syster	n (decentralised)		
Specific fan power:		0.19 0.18	
Maximum		0.7	OK
9 Summertime temperature			
Overheating risk (East An	iglia):	Slight	OK
Based on:			
Overshading:		Average or unknown	
Windows facing: South		4.77m²	
Windows facing: North		3.94m²	
Ventilation rate:		3.00	
Blinds/curtains:		Dark-coloured curtain or roller bli	ind
		Closed 100% of daylight hours	
10 Key features			
Doors U-value		1 W/m²K	
200.00 10.00			

### **Predicted Energy Assessment**

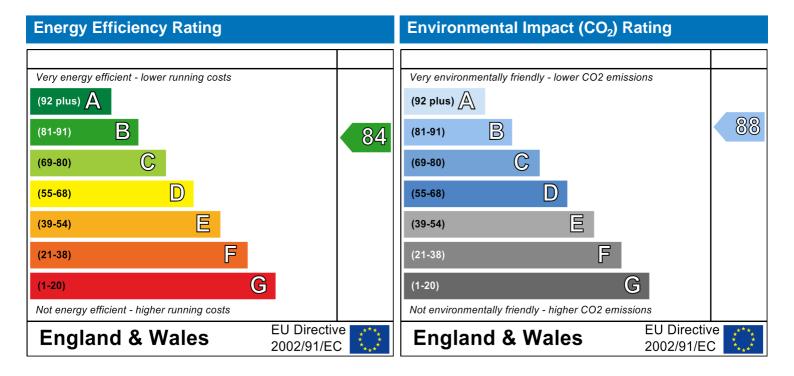


Plot 149 - Type A Tye Green Dwelling type:
Date of assessment:
Produced by:
Total floor area:

Ground floor Flat 20 February 2020 Matthew Stainrod 73.43 m<sup>2</sup>

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2012 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO2) emissions.



The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be.

The environmental impact rating is a measure of a home's impact on the environment in terms of carbon dioxide (CO2) emissions. The higher the rating the less impact it has on the environment.

### **SAP Input**



#### Property Details: 08-19-79354 Plot 149 - Type A

Address: Plot 149 - Type A, Tye Green

Located in: England Region: East Anglia

**UPRN**:

Date of assessment: 20 February 2020 Date of certificate: 26 February 2020

Assessment type: New dwelling design stage

Transaction type:

Tenure type:

Related party disclosure:

Thermal Mass Parameter:

Water use <= 125 litres/person/day:

New dwelling
Unknown

No related party
Calculated 189.65

True

PCDF Version: 455

#### Property description:

Dwelling type: Flat

Detachment:

Year Completed: 2020

Floor Location: Floor area:

Storey height:

Basement floor 73.43 m<sup>2</sup> 2.39 m

Living area: 25.81 m<sup>2</sup> (fraction 0.351)

Front of dwelling faces: East

#### Opening types:

Name: Source: Type: Glazing: Argon: Frame: Solid Front Manufacturer Wood Front Manufacturer Windows low-E, En = 0.05, soft coat Yes PVC-U Rear Manufacturer Windows low-E, En = 0.05, soft coat Yes PVC-U

Name:	Gap:	Frame Fa	ctor: g-value:	U-value:	Area:	No.
Front	mm	0.7	0	1	2.08	1
Front	16mm or more	0.7	0.63	1.2	4.77	1
Rear	16mm or more	0.7	0.63	1.2	3.94	1

Type-Name: Location: Orient: Width: Height: Name: Front Communal Wall East External Wall 0 Front South 0 Rear External Wall North 0

Overshading: Average or unknown

#### Opaque Elements:

Type:	Gross area:	Openings:	Net area:	U-value:	Ru value:	Curtain wall:	Карра:
External Element	<u>:S</u>						
External Wall	65.2	8.71	56.49	0.21	0	False	60
Communal Wall	17.64	2.08	15.56	0.27	0.43	False	60
Ground Floor	73.43			0.15			75
Internal Element	<u>s</u>						
Timber	210.32						9
Party Elements							
Ceiling	73.43						30

#### Thermal bridges

of Openings:

### **SAP Input**



Thermal bridges: User-defined (individual PSI-values) Y-Value = 0.0445

9.56

Length Psi-value Other lintels (including other steel lintels) 7.95 E2 [Approved] 0.3 Sill 5.57 0.022 E3 18.78 E4 Jamb 0.02 Ground floor (normal) 34.66 0.064 E5 Party floor between dwellings (in blocks of flats) 34.66 0.04 E7

E16

Ventilation:

Pressure test: Yes (As designed)

Ventilation: Decentralised whole house extract

Number of fans in Wetroom: Kitchen 1 Other 1

0.048

Ductwork: ,

Approved Installation Scheme: False

Number of chimneys: 0
Number of open flues: 0
Number of fans: 0
Number of passive stacks: 0
Number of sides sheltered: 2
Pressure test: 5

Main heating system:

Main heating system: Boiler systems with radiators or underfloor heating

Gas boilers and oil boilers

Fuel: mains gas

Info Source: Boiler Database

Database: (rev 455, product index 018203) Efficiency: Winter 86.7 % Summer: 89.9

Corner (normal)

Brand name: Potterton

Model: Assure

Model qualifier: 25 Combi

(Combi boiler)

Systems with radiators

Central heating pump: 2013 or later

Design flow temperature: Design flow temperature >45°C

Boiler interlock: Yes Delayed start

Main heating Control:

Main heating Control: Time and temperature zone control by suitable arrangement of plumbing and electrical

services

Control code: 2110

Secondary heating system:

Secondary heating system: None

Water heating:

Water heating: From main heating system

Water code: 901 Fuel: mains gas No hot water cylinder Solar panel: False

Others:

Electricity tariff: Standard Tariff
In Smoke Control Area: Unknown
Conservatory: No conservatory

Low energy lights: 100%

Terrain type: Low rise urban / suburban

EPC language: English

## **SAP Input**



Wind turbine: No
Photovoltaics: None
Assess Zero Carbon Home: No



User Details: **Assessor Name:** Matthew Stainrod Stroma Number: STRO023501 Stroma FSAP 2012 **Software Version: Software Name:** Version: 1.0.4.23 Property Address: 08-19-79354 Plot 149 - Type A Plot 149 - Type A, Tye Green Address: 1. Overall dwelling dimensions: Area(m²) Av. Height(m) Volume(m³) **Basement** 73.43 (1a) x 2.39 (2a) = 175.5 (3a) Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+....(1n)(4)73.43 Dwelling volume (3a)+(3b)+(3c)+(3d)+(3e)+....(3n) =175.5 (5) total m³ per hour main secondary other heating heating x 40 =Number of chimneys (6a) 0 0 x 20 =Number of open flues 0 O O 0 0 (6b) Number of intermittent fans x 10 =(7a) 0 0 x 10 =Number of passive vents (7b) 0 0 x 40 =Number of flueless gas fires (7c)Air changes per hour Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = $\div$  (5) = (8) If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16) Number of storeys in the dwelling (ns) (9)O Additional infiltration (10)[(9)-1]x0.1 =0 Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction (11)0 if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35 If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0 0 (12)If no draught lobby, enter 0.05, else enter 0 (13)0 Percentage of windows and doors draught stripped (14)0 Window infiltration  $0.25 - [0.2 \times (14) \div 100] =$ 0 (15)Infiltration rate (8) + (10) + (11) + (12) + (13) + (15) =O (16)Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area (17)5 If based on air permeability value, then  $(18) = [(17) \div 20] + (8)$ , otherwise (18) = (16)0.25 (18)Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used Number of sides sheltered (19)2  $(20) = 1 - [0.075 \times (19)] =$ Shelter factor (20)0.85  $(21) = (18) \times (20) =$ Infiltration rate incorporating shelter factor (21)0.21 Infiltration rate modified for monthly wind speed Jan Feb Sep Mar Apr Mav Jun Jul Aug Oct Nov Dec Monthly average wind speed from Table 7 (22)m =5.1 4.9 4.4 4.3 3.8 3.8 3.7 4 4.3 4.5 4.7

1.1

1.08

0.95

0.95

0.92

1

1.08

1.12

1.18

1.23

Wind Factor  $(22a)m = (22)m \div 4$ 

1.25

1.27

(22a)m



74.8page 2 of 389)

Average =  $Sum(39)_{1...12}/12=$ 

Adjusted infilt	ration rat	e (allowi	ing for sl	nelter an	d wind s	speed) =	(21a) x	(22a)m					
0.27	0.27	0.26	0.23	0.23	0.2	0.2	0.2	0.21	0.23	0.24	0.25	]	
Calculate effe		_	rate for t	he appli	cable ca	se							7,220
If exhaust air h			endix N. (2	(23a) = (23a	a) × Fmv (e	eguation (f	N5)) . othe	rwise (23b	) = (23a)			0.5	(23a
If balanced wit									) = (20a)			0.5	(23b
a) If balance		-	-	_					2h\m ı (	(22h) v [	1 (226)	0	(230
(24a)m= 0			0	0	0	0	0	$\frac{1}{0}$	0	0	0	]	(24a
b) If balance	ļ		ļ									j	(= :-
(24b)m= 0		0	0	0	0	0	0	0	0	0	0	1	(24b
c) If whole h												]	`
•	m < 0.5 >			•	-				.5 × (23k	o)			
(24c)m= 0.52	0.52	0.51	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	]	(240
d) If natural	ventilatio	on or wh	ole hous	se positiv	ve input	ventilatio	on from	loft				1	
•	m = 1, th			•	•				0.5]				
(24d)m= 0	0	0	0	0	0	0	0	0	0	0	0		(240
Effective air	r change	rate - er	nter (24a	) or (24k	o) or (24	c) or (24	d) in bo	x (25)				_	
(25)m= 0.52	0.52	0.51	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5		(25)
3. Heat losse	es and he	eat loss i	naramet	≏r·									
ELEMENT	Gros	SS	Openir	ıgs	Net Ar		U-val		AXU		k-value		
_	area	(m²)	m	) <sup>2</sup>	A ,r	m²	W/m2	2K 	(W/	K)	kJ/m²•	K kJ/	′K
Doors					2.08		1	=	2.08				(26)
Windows Typ	e 1				4.77	x1	/[1/( 1.2 )+	0.04] =	5.46				(27)
Windows Typ	e 2				3.94	х1	/[1/( 1.2 )+	0.04] =	4.51				(27)
Floor					73.43	3 X	0.15	=	11.014	5	75	5507.2	5 (28)
Walls Type1	65.	2	8.71		56.49	) x	0.21	=	11.86		60	3389.4	(29)
Walls Type2	17.6	64	2.08	3	15.56	3 x	0.24		3.76		60	933.6	(29)
Total area of	elements	s, m²			156.2	7							— (31)
Party ceiling					73.43	3				[	30	2202.9	(32b
Internal wall *	*				210.3	2				[	9	1892.88	3 (320
* for windows and	d roof wind	lows, use e	effective w	indow U-va			formula 1	/[(1/U-valu	ıe)+0.04] a	ו as given in	paragrapi		`
** include the are	as on both	sides of ir	nternal wai	ls and par	titions								
Fabric heat lo	ss, W/K	= S (A x	U)				(26)(30	) + (32) =				38.69	(33)
Heat capacity	Cm = S	(A x k )						((28).	(30) + (3	2) + (32a)	(32e) =	13926.03	(34)
Thermal mass	s parame	eter (TMF	P = Cm -	: TFA) ir	n kJ/m²K			= (34)	÷ (4) =			189.65	(35)
For design asses				construct	ion are no	t known pr	ecisely the	e indicative	e values of	TMP in T	able 1f		
can be used inste				uoina An	n an div l	/							7,00
Thermal bridg					-	^						6.95	(36)
if details of therm Total fabric he		are HOLKI	10VVII (30) =	- u.uu x (3	'' <i>')</i>			(33) +	(36) =			45.64	(37)
Ventilation he		alculated	d monthl	V					= 0.33 × (	(25)m x (5	)	70.07	``
Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	1	
(38)m= 30.17	29.86	29.55	28.96	28.96	28.96	28.96	28.96	28.96	28.96	28.96	28.96	1	(38)
Heat transfer	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>				ļ		1	. ,
(39)m= 75.81	75.5	75.2	74.6	74.6	74.6	74.6	74.6	74.6	= (37) + ( 74.6	74.6	74.6	1	
13.01	75.5	10.2	14.0	/4.0	14.0	14.0	14.0	14.0	14.0	74.0	14.0	ļ	_

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leat lo	ss para	meter (F	ILP), W/	m²K					(40)m	= (39)m ÷	· (4)			
10)m=	1.03	1.03	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.02		_
umbe	or of dov	o in moi	nth (Tabl	lo 1o\					1	Average =	Sum(40) <sub>1</sub> .	12 /12=	1.02	(40
iumbe	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
41)m=	31	28	31	30	31	30	31	31	30 30	31	30	31		(4 <sup>2</sup>
.,														`
1 Ws	iter heat	ing ener	gy requi	rement:								kWh/ye	ar·	
T. VVC	itor ricat	ing chei	gy roqui	rement.								RVVII/yC	ar.	
if TF	ed occu A > 13.9 A £ 13.9	0, N = 1	N + 1.76 x	[1 - exp	(-0.0003	349 x (TF	FA -13.9	)2)] + 0.0	0013 x ( <sup>-</sup>	ΓFA -13.		33		(4)
nnua	l averag	e hot wa	ater usag hot water							se target o		.45		(4
ot more	e that 125	litres per p	oerson per	day (all w	ater use, l	hot and co	ld)							
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
ot wate	er usage ir	n litres per	day for ea	ach month	Vd,m = fa	ctor from	Table 1c x	(43)						
4)m=	98.4	94.82	91.24	87.66	84.09	80.51	80.51	84.09	87.66	91.24	94.82	98.4		_
nerav (	content of	hot water	used - cal	culated m	onthly – 1	100 v Vd r	n v nm v F	Tm / 3600			m(44) <sub>112</sub> = ables 1b, 1	L	1073.43	(4
	-						<del> </del>		<del> </del>	· ·	·			
5)m=	145.92	127.62	131.7	114.82	110.17	95.07	88.09	101.09	102.3	119.22	130.13	141.32	1407.44	(4
instant	taneous w	ater heatii	ng at point	of use (no	hot water	storage),	enter 0 in	boxes (46)		10tai = Su	m(45) <sub>112</sub> =	L	1407.44	(-
6)m=	21.89	19.14	19.75	17.22	16.53	14.26	13.21	15.16	15.34	17.88	19.52	21.2		(4
/ater	storage	loss:									<u> </u>	<u> </u>		
torag	e volum	e (litres)	includin	ig any so	olar or W	/WHRS	storage	within sa	ame ves	sel		0		(4
	•	•	nd no ta		•			` '		(01 ! /	(47)			
	vise it no storage		hot wate	er (tnis in	iciuaes i	nstantar	eous co	ilod idmo	ers) ente	er o in (	47)			
	-		eclared l	oss facto	or is kno	wn (kWh	n/day):					0		(4
•			m Table			`	3,					0		(4
•			storage		ear			(48) x (49)	) =			0		` (5
•			eclared o	-		or is not	known:					<u> </u>		(-
		•	factor fr		e 2 (kWl	h/litre/da	ıy)					0		(5
	nunity h e factor	•	ee sectio	on 4.3										/-
			m Table	2h							<b>—</b>	0		(5 (5
			storage		aar			(47) x (51)	) x (52) x (	53) =				(5
٠.	(50) or (		•	, KVVII/ y C	zai			(47) X (01)	/ X (02) X (	00) =		0		(5
	. , ,	, ,	, culated f	or each	month			((56)m = (	55) × (41):	m				•
66)m=	0	0	0	0	0	0	0	0	0	0	0	0		(5
	-		-					_		_	_	m Appendix	κН	,,
57)m=	0	0	0	0	0	0	0	0	0	0	0	0		(5
	v oirouit	loce (e-	nough fro	m Toble	. 2				<u> </u>	<u> </u>		0		(5
	•	,	inual) fro culated f			59)m = (	(58) <u>–</u> 36	35 x (41)	m			·		(0
	-				•	•	. ,	, ,		r thermo	stat)			
(mod		idotoi ii	on rab											



Combi loss calcula	ted for each	n month	(61)m =	(60) ÷ 3	65 × (41	)m						
(61)m= 14.55 13		14.06	14.52	14.05	14.51	14.52	14.05	14.53	14.07	14.55		(61)
Total heat required	for water h	eating ca	alculated	l for eac	h month	(62)m	= 0.85 × (	(45)m +	(46)m +	(57)m +	ı (59)m + (61)m	
(62)m= 160.47 140		128.88	124.69	109.11	102.61	115.61		133.75	144.2	155.86		(62)
Solar DHW input calcul	ated using App	pendix G o	r Appendix	: H (negati	ve quantity	y) (enter	0' if no sola	r contribut	ion to wate	er heating)	I	
(add additional line	s if FGHRS	and/or \	NWHRS	applies	, see Ap	pendix	G)					
(63)m= 0	0	0	0	0	0	0	0	0	0	0		(63)
Output from water	neater											
(64)m= 160.47 140	76 146.23	128.88	124.69	109.11	102.61	115.61	116.35	133.75	144.2	155.86		_
-						Ou	tput from w	ater heate	r (annual) <sub>1</sub>	I12	1578.52	(64)
Heat gains from wa	ter heating	, kWh/m	onth 0.2	5 ´ [0.85	× (45)m	+ (61)	m] + 0.8 >	k [(46)m	+ (57)m	+ (59)m	]	
(65)m= 52.16 45	72 47.42	41.69	40.26	35.12	32.92	37.24	37.53	43.27	46.79	50.62		(65)
include (57)m in	calculation	of (65)m	only if o	ylinder i	s in the	dwelling	g or hot w	ater is f	rom com	munity h	eating	
5. Internal gains	see Table	5 and 5a	):									
Metabolic gains (T	able 5), Wa	tts									_	
Jan F	eb Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
(66)m= 139.59 139	59 139.59	139.59	139.59	139.59	139.59	139.59	139.59	139.59	139.59	139.59		(66)
Lighting gains (cal	ulated in A	ppendix	L, equat	ion L9 o	r L9a), a	lso see	Table 5					
(67)m= 50.89 45	2 36.76	27.83	20.8	17.56	18.98	24.66	33.1	42.03	49.06	52.3		(67)
Appliances gains (	calculated in	n Append	dix L, eq	uation L	13 or L1	3a), als	so see Ta	ble 5	-	-		
(68)m= 306.22 309	.4 301.39	284.34	262.82	242.6	229.09	225.91	233.92	250.96	272.48	292.71		(68)
Cooking gains (cal	culated in A	ppendix	L, equat	ion L15	or L15a	), also s	see Table	5	-		•	
(69)m= 51.29 51	29 51.29	51.29	51.29	51.29	51.29	51.29	51.29	51.29	51.29	51.29		(69)
Pumps and fans g	ins (Table	5a)			-		-		-		•	
(70)m= 3	3	3	3	3	3	3	3	3	3	3		(70)
Losses e.g. evapo	ation (nega	tive valu	es) (Tab	le 5)	-		-		-	-		
(71)m= -93.06 -93	06 -93.06	-93.06	-93.06	-93.06	-93.06	-93.06	-93.06	-93.06	-93.06	-93.06		(71)
Water heating gair	s (Table 5)	-		-	-	-	-	-	-	-		
(72)m= 70.1 68	03 63.74	57.9	54.12	48.78	44.25	50.06	52.12	58.16	64.98	68.04		(72)
Total internal gain	ıs =			(66)	)m + (67)m	n + (68)m	+ (69)m +	(70)m + (7	'1)m + (72)	)m	•	
(73)m= 528.02 523	44 502.7	470.89	438.55	409.75	393.12	401.44	419.96	451.97	487.34	513.86		(73)
6. Solar gains:												
Solar gains are calcul	ited using sola	ar flux from	Table 6a	and assoc	ciated equa	ations to	convert to th	e applicat	ole orientat	tion.		
Orientation: Acce		Area		Flu			g_ Table 6b	_	FF		Gains	
Table		m²		Ta	ble 6a	, _	Table 6b	_ '	able 6c		(W)	,
	).77 ×	3.9	94	X 1	10.63	X	0.63	x	0.7	=	12.8	(74)
	).77 ×	3.9	94	x	20.32	x	0.63	x	0.7	=	24.47	(74)
	).77 ×	3.9	94	x	34.53	x	0.63	x	0.7	=	41.58	(74)
	).77 ×	3.9	94	X	55.46	x	0.63	x	0.7	=	66.79	(74)
North 0.9x	).77 ×	3.9	94	x	74.72	x	0.63	x	0.7	=	89.97	(74)



	_											_			_		_
North	0.9x	0.77	X	3.9	94	X	7	'9.99	X		0.63	X	0.7	-	• <u>L</u>	96.31	(74)
North	0.9x	0.77	x	3.9	94	X	7	4.68	X		0.63	X	0.7	=		89.92	(74)
North	0.9x	0.77	X	3.9	94	X	5	9.25	X		0.63	X	0.7	=		71.34	(74)
North	0.9x	0.77	X	3.9	94	X	4	1.52	X		0.63	X	0.7	=		49.99	(74)
North	0.9x	0.77	X	3.9	)4	X	2	4.19	X		0.63	X	0.7	=	<u> </u>	29.13	(74)
North	0.9x	0.77	X	3.9	94	X	1	3.12	x		0.63	X	0.7	-		15.8	(74)
North	0.9x	0.77	X	3.9	94	X		3.86	X		0.63	X	0.7	=		10.67	(74)
South	0.9x	0.77	X	4.7	77	X	4	6.75	X		0.63	x	0.7	=	- [	68.15	(78)
South	0.9x	0.77	X	4.7	77	X	7	6.57	X		0.63	x	0.7	=	-	111.62	(78)
South	0.9x	0.77	Х	4.7	77	X	9	7.53	X		0.63	x	0.7	=		142.18	(78)
South	0.9x	0.77	х	4.7	77	X	1	10.23	x		0.63	×	0.7		• <u> </u>	160.7	(78)
South	0.9x	0.77	X	4.7	77	X	1	14.87	x		0.63	x	0.7	╡ -	▫┌	167.46	(78)
South	0.9x	0.77	x	4.7	77	X	1	10.55	x		0.63	x	0.7		▫┌	161.15	(78)
South	0.9x	0.77	X	4.7	77	X	1	08.01	X		0.63	x	0.7	<u> </u>	▫┌	157.46	(78)
South	0.9x	0.77	х	4.7	77	X	1	04.89	x		0.63	x	0.7	=	•	152.91	(78)
South	0.9x	0.77	х	4.7	77	X	1	01.89	x		0.63	×	0.7		▫┌	148.53	(78)
South	0.9x	0.77	Х	4.7	77	X	8	2.59	x		0.63	×	0.7		▫┢	120.39	(78)
South	0.9x	0.77	х	4.7	77	X	5	5.42	x		0.63	×	0.7		▗▕▔	80.79	(78)
South	0.9x	0.77	×	4.7	77	X	<u> </u>	40.4	x		0.63	= x	0.7		▫┌	58.89	(78)
Solar ga (83)m= Total ga	80.96	136.09	183.76	227.48	257.42	2	57.47 83)m	247.38	(83)m 224		m(74)m . 198.52	<mark>(82)m</mark> 149.5		69.57			(83)
	608.98	659.53	686.46	698.37	695.98	<del>,</del>	67.22	640.5	625	5.7	618.47	601.4	9 583.92	583.43	3		(84)
7 Mea	n inter	nal temp	erature	(heating	Seasor	7)											
		during h		`			area :	from Tab	ole 9	Th1	(°C)				Т	21	(85)
•		tor for ga	•			-			J.O 0,	,	( 0)				L		
	Jan	Feb	Mar	Apr	May	Ť	Jun	Jul	A	ug	Sep	Oct	Nov	Dec	$\Box$		
(86)m=	0.98	0.97	0.95	0.9	0.82	+	0.66	0.5	0.5	<del>-</del>	0.73	0.9	0.96	0.98	$\exists$		(86)
` ′ ∟	ntorno	Ltompor			ļ	مالہ	w oto	no 2 to 7						ļ			
	19.91	temper 20.06	20.29	20.56	20.79	$\overline{}$	0.94	20.99	20.	-	9C) 20.9	20.62	2 20.23	19.89	$\Box$		(87)
` '					<u> </u>			<u> </u>					20.20	1 .0.00			()
· -		during h			i	1		1		<del>.</del>	<u> </u>	20.07	7 20.07	20.07	$\Box$		(88)
(88)m=	20.06	20.06	20.06	20.07	20.07		20.07	20.07	20.	07	20.07	20.07	20.07	20.07			(00)
Г		tor for g		1		1		1	r –						_		
(89)m=	0.97	0.96	0.94	0.88	0.77	(	0.58	0.4	0.4	13	0.66	0.88	0.96	0.98			(89)
Mean_i	nterna	temper	ature in	the rest	of dwel	ling	T2 (f	ollow ste	ps 3	to 7	in Tabl	e 9c)			_		
(90)m=	18.63	18.84	19.16	19.55	19.86	2	20.02	20.06	20.	06	19.99	19.64		18.61			(90)
											f	LA = Liv	ving area ÷ (	4) =		0.35	(91)
Mean i	nterna	temper	ature (fo	r the wh	ole dwe	ellin	g) = f	$LA \times T1$	+ (1	_ fL/	A) × T2						
_	nterna 19.08	19.27	ature (fo 19.56	r the wh	ole dwe 20.19	$\overline{}$	g) = f 20.35	20.39	+ (1 20.		A) × T2 20.31	19.99	19.49	19.06			(92)



			ı		<del> </del>		i		ı				1	(22)
(93)m=	18.93	19.12	19.41	19.75	20.04	20.2	20.24	20.23	20.16	19.84	19.34	18.91		(93)
			uirement							,			• .	
				mperatui using Ta		ed at ste	ep 11 of	Table 9	b, so tha	it Ti,m=(	76)m an	d re-calc	:ulate	
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
Utilisa	ation fac	tor for g	ains, hm	n:									-	
(94)m=	0.97	0.95	0.93	0.87	0.77	0.59	0.42	0.45	0.67	0.87	0.95	0.97		(94)
Usefu	ıl gains,	hmGm	, W = (94	4)m x (84	4)m			•		•	•		ı	
(95)m=	588.55	627.69	635.34	608.7	534.58	396.55	267.95	281.24	415.28	521.82	552.49	566.52		(95)
Montl	hly avera	age exte	rnal tem	perature	from Ta	able 8	•	•	•	•	•	•	I	
(96)m=	4.3	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2		(96)
Heat	loss rate	for mea	an intern	al tempe	erature,	Lm , W =	=[(39)m	x [(93)m	– (96)m	]		•	J	
(97)m=	1109	1073.81	970.63	809.69	621.97	417.5	271.38	286.05	451.98	688.98	913.19	1097.17		(97)
Spac	e heatin	g require	ement fo	r each n	nonth, k\	/Vh/mont	th = 0.02	24 x [(97	)m – (95	5)m] x (4	1)m		1	
(98)m=	387.21	299.8	249.46	144.72	65.01	0	0	0	0	124.36	259.71	394.8		
			ļ	ļ	<u> </u>		<u>[</u>	<u>.                                    </u>	l per year	(kWh/vea	) = Sum(9	8)15912 =	1925.07	(98)
0				1-10/1- /	26				, , , ,	( :,	, (-	- /		]
Spac	e neatin	g require	ement in	kWh/m²	/year								26.22	(99)
9a. En	ergy rec	uiremer	nts – Ind	ividual h	eating sy	ystems i	ncluding	micro-C	CHP)					
Spac	e heatir	ıg:												_
Fract	ion of sp	ace hea	at from s	econdar	y/supple	mentary	system						0	(201)
Fract	ion of sp	ace hea	at from m	nain syst	em(s)			(202) = 1	- (201) <b>=</b>				1	(202)
Fract	ion of to	tal heati	ng from	main sys	stem 1			(204) = (2	02) <b>x</b> [1 –	(203)] =			1	(204)
			•	ing syste									89.9	(206)
	•	-		•			. 0/							╣ .
EIIICI	ency of s		· · ·	ementar	y neating	g system							0	(208)
_	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/yea	ır
Spac		<u> </u>	<del>- `</del>	alculate	d above)	)						1	I	
	387.21	299.8	249.46	144.72	65.01	0	0	0	0	124.36	259.71	394.8		
(211)m	$1 = \{[(98)]$	)m x (20	(4)] } x 1	00 ÷ (20	06)								_	(211)
	430.71	333.48	277.49	160.97	72.32	0	0	0	0	138.34	288.88	439.16		
			•				•	Tota	l (kWh/yea	ar) =Sum(2	211),5,101	<u>.                                    </u>	2141.35	(211)
Spac	e heatin	a fuel (s	econdar	y), kWh/	month									_
		• '	00 ÷ (20											
(215)m=		0	0	0	0	0	0	0	0	0	0	0		
			!				<u> </u>	Tota	l II (kWh/yea	ar) =Sum(2	1 215) <sub>15.101</sub>	=	0	(215)
Water	heating											l		]` ′
	_		ter (calc	ulated al	hove)									
Catpa	160.47	140.76	146.23	128.88	124.69	109.11	102.61	115.61	116.35	133.75	144.2	155.86		
Efficie	ncy of w	ater hea	ıter		<u> </u>		<u> </u>	<u> </u>	ļ	<u> </u>	<u>!</u>		86.7	(216)
(217)m=		88.85	88.69	88.36	87.77	86.7	86.7	86.7	86.7	88.21	88.73	88.97		J` ´ (217)
` ,					J,	50.7		1	1	1 30.21	1 50.75	55.57	İ	(===)
		•	kWh/mo (217) ÷ (											
, ,	180.43	158.42	164.88	145.85	142.06	125.85	118.35	133.34	134.2	151.62	162.52	175.18		
			<u> </u>		<u> </u>		<u> </u>	<u> </u>	l = Sum(2		<u> </u>	-	1792.7	(219)
Δnnus	al totals								,		Wh/yeaı	- -	kWh/year	۱٬۵۰۵)
		fuel use	ed. main	system	1					ĸ	• • i ii y <del>c</del> ai	<u> </u>	2141.35	1
Space	. routing	436	, mani	3,3(3)11	•								2141.00	J



Water heating fuel used			1792.7
Electricity for pumps, fans and electric keep-hot			
mechanical ventilation - balanced, extract or po	ositive input from outside	51.8	(230a)
central heating pump:		30	(230c)
boiler with a fan-assisted flue		45	(230e)
Total electricity for the above, kWh/year	sum o	of (230a)(230g) =	126.82 (231)
Electricity for lighting			359.46 (232)
10a. Fuel costs - individual heating systems:			
	<b>Fuel</b> kWh/year	Fuel Price (Table 12)	Fuel Cost £/year
Space heating - main system 1	(211) x	3.48 × 0.01	= 74.52 (240)
Space heating - main system 2	(213) x	0 x 0.01	= 0 (241)
Space heating - secondary	(215) x	13.19 × 0.01	= 0 (242)
Water heating cost (other fuel)	(219)	3.48 x 0.01	= 62.39 (247)
Pumps, fans and electric keep-hot	(231)	13.19 x 0.01	= 16.73 (249)
(if off-peak tariff, list each of (230a) to (230g) se Energy for lighting	parately as applicable an	d apply fuel price according 13.19 × 0.01	
Additional standing charges (Table 12)			120 (251)
Appendix Q items: repeat lines (253) and (254) and (254)(245)(2	as needed 247) + (250)(254) =		321.05 (255)
			321.05 (255)
Total energy cost (245)(2			321.05 (255) 0.42 (256)
Total energy cost (245)(2  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)			
Total energy cost (245)(2  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)	247) + (250)(254) =		0.42 (256)
Total energy cost (245)(2  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF) (255) x (245)(2	(256)] ÷ [(4) + 45.0] =		0.42 (256) 1.14 (257)
Total energy cost (245)(2  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF) [(255) x (255) x	(256)] ÷ [(4) + 45.0] =	Emission factor kg CO2/kWh	0.42 (256) 1.14 (257)
Total energy cost (245)(2  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF) [(255) x (255) x	(256)] ÷ [(4) + 45.0] =  ms including micro-CHP  Energy		0.42 (256) 1.14 (257) 84.12 (258)  Emissions
Total energy cost  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF) [(255) x ( SAP rating (Section 12)  12a. CO2 emissions - Individual heating system	247) + (250)(254) =  (256)] ÷ [(4) + 45.0] =  ms including micro-CHP  Energy kWh/year	kg CO2/kWh	0.42 (256) 1.14 (257) 84.12 (258)  Emissions kg CO2/year
Total energy cost  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF) [(255) x ( SAP rating (Section 12)  12a. CO2 emissions - Individual heating system  Space heating (main system 1)	247) + (250)(254) =  (256)] ÷ [(4) + 45.0] =  ms including micro-CHP  Energy kWh/year (211) x	kg CO2/kWh	0.42 (256) 1.14 (257) 84.12 (258)  Emissions kg CO2/year 462.53 (261)
Total energy cost  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF)  SAP rating (Section 12)  12a. CO2 emissions – Individual heating system  Space heating (main system 1)  Space heating (secondary)	247) + (250)(254) =  (256)] ÷ [(4) + 45.0] =  ms including micro-CHP  Energy kWh/year (211) x (215) x	kg CO2/kWh  0.216 =  0.519 =  0.216 =	0.42 (256) 1.14 (257) 84.12 (258)  Emissions kg CO2/year 462.53 (261) 0 (263)
Total energy cost  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF)  SAP rating (Section 12)  12a. CO2 emissions - Individual heating system  Space heating (main system 1)  Space heating (secondary)  Water heating	247) + (250)(254) =  (256)] ÷ [(4) + 45.0] =  ms including micro-CHP  Energy kWh/year (211) x (215) x (219) x (261) + (262) + (263) + (263)	kg CO2/kWh  0.216 =  0.519 =  0.216 =	0.42 (256) 1.14 (257) 84.12 (258)  Emissions kg CO2/year 462.53 (261) 0 (263) 387.22 (264)
Total energy cost  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF)  SAP rating (Section 12)  12a. CO2 emissions - Individual heating system  Space heating (main system 1)  Space heating (secondary)  Water heating  Space and water heating	247) + (250)(254) =  (256)] ÷ [(4) + 45.0] =  ms including micro-CHP  Energy kWh/year (211) x (215) x (219) x (261) + (262) + (263) + (263)	kg CO2/kWh  0.216 =  0.519 =  0.216 =	0.42 (256) 1.14 (257) 84.12 (258)  Emissions kg CO2/year 462.53 (261) 0 (263) 387.22 (264) 849.75 (265)
Total energy cost  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF) [(255) x ( SAP rating (Section 12)  12a. CO2 emissions - Individual heating system  Space heating (main system 1)  Space heating (secondary)  Water heating  Space and water heating  Electricity for pumps, fans and electric keep-hot	247) + (250)(254) =  (256)] ÷ [(4) + 45.0] =  ms including micro-CHP  Energy kWh/year (211) x (215) x (219) x (261) + (262) + (263) + (263) + (2631) x	kg CO2/kWh  0.216 =  0.519 =  0.216 =  0.519 =	0.42 (256) 1.14 (257) 84.12 (258)  Emissions kg CO2/year  462.53 (261) 0 (263) 387.22 (264) 849.75 (265) 65.82 (267)
Total energy cost  11a. SAP rating - individual heating systems  Energy cost deflator (Table 12)  Energy cost factor (ECF) [(255) x ( SAP rating (Section 12)  12a. CO2 emissions - Individual heating system  Space heating (main system 1)  Space heating (secondary)  Water heating  Space and water heating  Electricity for pumps, fans and electric keep-hot  Electricity for lighting	247) + (250)(254) =  (256)] ÷ [(4) + 45.0] =  ms including micro-CHP  Energy kWh/year (211) x (215) x (219) x (261) + (262) + (263) + (263) + (2631) x	kg CO2/kWh  0.216 =  0.519 =  0.216 =  0.519 =  0.519 =	0.42 (256) 1.14 (257) 84.12 (258)  Emissions kg CO2/year  462.53 (261) 0 (263) 387.22 (264) 849.75 (265) 65.82 (267) 186.56 (268)



40-	Primary	
	Primary	
Joa.	ı ıllılalv	LIICIUV

	<b>Energy</b> kWh/year	Primary factor	<b>P. Energy</b> kWh/year
Space heating (main system 1)	(211) x	1.22	2612.44 (261)
Space heating (secondary)	(215) x	3.07	0 (263)
Energy for water heating	(219) x	1.22	2187.09 (264)
Space and water heating	(261) + (262) + (263) + (264) =		4799.54 (265)
Electricity for pumps, fans and electric keep-hot	(231) x	3.07	389.35 (267)
Electricity for lighting	(232) x	0 =	1103.55 (268)
'Total Primary Energy	sum	of (265)(271) =	6292.43 (272)
Primary energy kWh/m²/year	(272	2) ÷ (4) =	85.69 (273)

### **SAP 2012 Overheating Assessment**



Calculated by Stroma FSAP 2012 program, produced and printed on 26 February 2020

#### Property Details: 08-19-79354 Plot 149 - Type A

Dwelling type:FlatLocated in:EnglandRegion:East Anglia

Cross ventilation possible:YesNumber of storeys:1Front of dwelling faces:East

Overshading: Average or unknown

Overhangs: None

Thermal mass parameter: Calculated 189.65

**Night ventilation:** False

Blinds, curtains, shutters:

Ventilation rate during hot weather (ach):

Dark-coloured curtain or roller blind
3 (Windows open half the time)

Overheating Details:

Summer ventilation heat loss coefficient: 173.74 (P1)

Transmission heat loss coefficient: 45.6

Summer heat loss coefficient: 219.38 (P2)

Overhangs:

Orientation: Ratio: Z\_overhangs:

South (Front) 0 1 North (Rear) 0 1

Solar shading:

Orientation:	Z blinds:	Solar access:	Overhangs:	Z summer:	
South (Front)	0.85	0.9	1	0.76	(P8)
North (Rear)	0.85	0.9	1	0.76	(P8)

Solar gains

Orientation		Area	Flux	<b>g</b> _	FF	Shading	Gains
South (Front)	0.9 x	4.77	114.84	0.63	0.7	0.76	166.32
North (Rear)	0.9 x	3.94	82.12	0.63	0.7	0.76	98.24
						Total	264 57 <b>(P3/P4)</b>

#### Internal gains:

	June	July	August	
Internal gains	406.75	390.12	398.44	
Total summer gains	685.07	654.69	639.31	(P5)
Summer gain/loss ratio	3.12	2.98	2.91	(P6)
Mean summer external temperature (East Anglia)	15.4	17.6	17.6	
Thermal mass temperature increment	0.67	0.67	0.67	
Threshold temperature	19.2	21.26	21.19	(P7)
Likelihood of high internal temperature	Not significant	Slight	Slight	

Assessment of likelihood of high internal temperature: Slight